

A Unidirectional Hybrid HVDC Transmission System Based on Diode Rectifier and Full-bridge MMC

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Abstract—To reduce the cost of bulk power transmission using voltage source converter HVDC technology, a unidirectional hybrid converter is proposed, where a diode rectifier and a modular multilevel converter (MMC) based on full-bridge (FB) submodules are connected in series on DC side. The FB-MMC controls its DC voltage to regulate the transmitted power. The majority of the power transmission is via the diode rectifier considering its cost and efficiency superiority and only low power rating FB-MMC is required. A thyristor valve is equipped at the DC side of the FB-MMC to prevent potential overcharge of the FB submodules during DC faults. Compared to conventional MMCs, losses can potentially be reduced by around 20%. An active power controller is proposed to regulate the DC voltage of the FB-MMC so as to control the transmitted power. With the inverter station controlling its DC terminal voltage constant, the FB-MMC increases the output DC voltage to increase the transmitted power and, vice versa. To alleviate overvoltage of the HVDC link during AC grid faults of the inverter station, a dynamic DC voltage limiter is designed to actively reduce the DC output voltage of the FB-MMC. Simulation results confirm the proposed converter operation and control.

Index Terms—active power control, diode rectifier HVDC (DR-HVDC), fault ride-through, HVDC transmission, full-bridge (FB) based modular multilevel converter (MMC).

I. INTRODUCTION

High-voltage DC (HVDC) transmission systems based on modular multilevel converters (MMCs) have developed rapidly due to their significant advantages. The most widely used MMC configuration is based on the half-bridge (HB) submodule (SM), whereas other MMC topologies have been proposed, e.g. MMCs based on the full-bridge (FB) SM [1], clamp double (CD) SM [2], and mixed SM [3], alternate-arm multilevel converters (AACs) [4], hybrid cascaded MMC [5], etc.

Diode rectifier (DR) based HVDC systems have recently received notable interest for integrating large offshore wind farms [6-8]. By replacing the MMC offshore station with diode rectifier, the volume and weight of the offshore platform can be significantly reduced. In addition, it also leads to substantial reduction in the transmission losses and the total cost, e.g. 20% and 30% respective reductions as quoted in [6, 7].

A voltage and frequency control of the offshore wind turbines connected with DR-HVDC system is presented in [9],

which proves that such solution is technically feasible in steady state and transients. The fault ride-through capability of DR-HVDC connected with offshore wind farm is further validated in [10-13]. However, the wind turbines in DR-HVDC systems need to operate in grid forming mode to build up the offshore AC network and the conventional wind turbines operating on grid following mode cannot be used for the DR-HVDC systems. In addition, the AC voltage magnitude of the network connected to DR-HVDC has to vary in order to regulate the active power transmission.

To address this issue, various hybrid topologies have been proposed. In [14], a two-level voltage source converter (VSC) is connected in series with the DR on DC side and controls the offshore AC voltage constant to transmit the generated wind power to onshore. The two-level VSC also compensates reactive power and suppresses harmonics generated by the DR. Reference [15] proposes to connect the cascaded H-bridge (CHB) converter with the DR on AC side, which only controls the frequency of the offshore AC network while the magnitude remains uncontrolled and is intrinsically clamped by the DR. Such control is different to the conventional control of static synchronous compensators (STATCOMs) where reactive power is generated through regulation of the AC voltage magnitude. The AC filter of the DR is removed and all of the reactive power and harmonics generated by the DR are compensated by the CHB converter. However, the CHB converter needs to be rated over 30% of the power rating of the DR-HVDC link, leading to high capital cost. In [16], the DR and MMC are connected in parallel on AC sides to optimize the power flow distribution between these two HVDC links and improve availability of the parallel connected HVDC systems during faults. The MMC is connected in parallel with the DR on both AC and DC sides in [17] to energize the offshore AC grid and wind turbines during start-up and control the offshore frequency during normal operation. However, the parallel connected VSC needs to be rated at the nominal DC voltage of the DR. In [18], cascaded FB SMs are connected at the VSC DC output to reduce the DC voltage rating of the parallel connected VSC. However, LC filter is required to constrain high frequency circulating currents between the VSC and DR.

The DR-HVDC systems in the aforementioned references are used for offshore wind energy transmission, where the offshore network is formed either by wind turbines [9-13] or by additional converters [14, 15, 18], and the AC voltage magnitude can be varied by the system. This paper aims to extend the DR concept to onshore application, where the AC voltage is independent of the transmission system, considering that the power flow of HVDC systems often has unidirectional characteristics when transmitting power from large power plants to load centers [19, 20]. The main contributions are:

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- A hybrid HVDC converter is proposed, where a high power rating DR is connected with a low power rating FB-MMC in series on the DC side, whilst a thyristor valve is in parallel with the FB-MMC for DC fault protection. The majority of the power transmission is via the DR considering its low cost and high efficiency while the FB-MMC is used to control the transmitted power by regulating the overall DC voltage generated by the two converters.
- A simple power-DC voltage (P - V_{dc}) control scheme is proposed to regulate the DC voltage of the FB-MMC so as to control the transmitted power of the HVDC link. A dynamic DC voltage limiter is introduced to actively reduce the DC output voltage of the FB-MMC to alleviate DC overvoltage of the HVDC link during AC grid faults of the inverter station.

The paper is organized as follows. The layout of the hybrid HVDC converter and its control strategy are proposed in Section II. In Section III, the design principles of the proposed topology and its efficiency superiority as well as economic benefits are presented. The proposed topology and its control strategy are assessed in Section IV and finally, Section V draws conclusions.

II. PROPOSED HYBRID HVDC SYSTEM BASED ON DIODE RECTIFIER AND FB-MMC

A. Converter Topology

Fig. 1 shows a generic version of the proposed hybrid HVDC converter comprising a diode rectifier bridge and FB SM based MMC (DFB-MMC). As seen, its main power stage consists of series connection of a high power 12-pulse DR bridge and a low power FB-MMC on their DC sides, while their AC sides are connected in parallel through interface transformers. Filters are connected on the DR AC side for reactive power compensation and harmonic suppression [6, 21]. Thyristor valve S_1 is connected in parallel with the FB-MMC on its DC side for DC fault protection, as will be detailed later. The DR and FB-MMC are designed such that the majority of the transmitted power is through the DR taking the advantage of its lower cost and high efficiency compared to MMCs while the low power rating FB-MMC is used to control the transmitted power of the whole hybrid HVDC system by regulating its DC voltage.

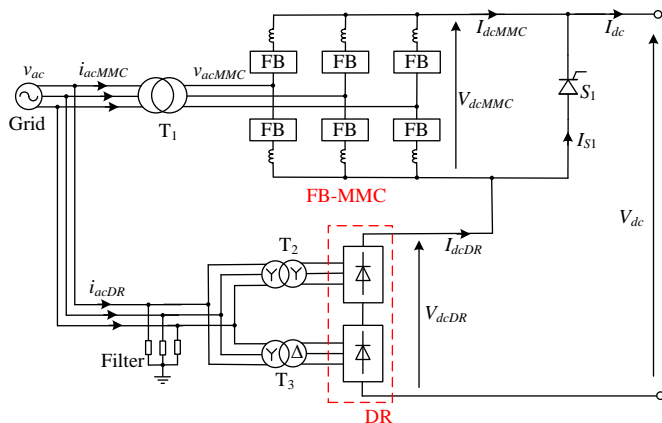


Fig. 1. Proposed hybrid HVDC converter based on diode rectifier and full-bridge MMC.

During normal operation, the thyristor valve S_1 is off and the FB-MMC is connected in-series with the DR to transmit power. The voltage across S_1 equals to the nominal FB-MMC DC voltage V_{dcMMC} .

In the event of DC faults, the FB-MMC is quickly blocked after fault detection, which then provides negative blocking voltage to its AC side to fast extinguish AC fault current. However, if the thyristor valve S_1 is not activated, the fault current fed from the DR AC side will flow through and charge the SMs of the FB-MMC, as indicated by the dashed lines in Fig. 2. This leads to overvoltage of the FB SM capacitors. Thus, the thyristor valve S_1 is activated in addition to the blocking of the FB-MMC after fault detection as aforementioned. Therefore, all the DC fault current from the DR I_{dcDR} flows through the thyristor S_1 and the FB-MMC is bypassed, as illustrated by the solid lines in Fig. 2. The AC circuit breakers (ACCBs) equipped at the AC terminals of the DR and FB-MMC then open for fault protection. The power transmission of the HVDC station is interrupted during DC faults, in a similar way as systems based on conventional HB-MMCs protected by ACCBs [22, 23]. Such protection arrangement is much cheaper than those using fast acting DC circuit breakers but may not be preferred for multi-terminal HVDC systems due to its relatively slow action.

Due to the fast protection response, the IGBTs in the FB-MMC can be quickly blocked and the contribution of DC fault current from SM capacitor discharging is thus limited. Similar to conventional HB-MMCs, the fault currents of the proposed converter are mainly fed from the grid through the DR.

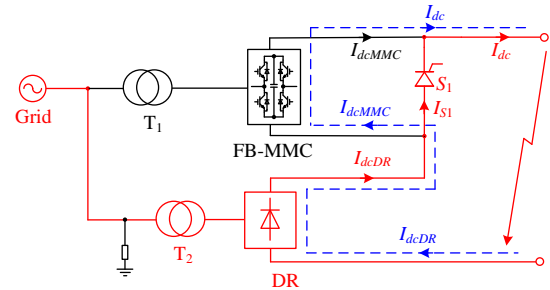


Fig. 2. Single-phase illustration of fault current path during DC faults.

B. Operation Principle

The HVDC link based on the proposed topology is illustrated in Fig. 3, where the DFB-MMC and conventional HB-MMC are adopted as the rectifier and inverter stations, respectively. The proposed DFB-MMC controls the transmitted power while the HB-MMC of the inverter station operates on DC voltage control mode and regulates its DC terminal voltage at the rated value.

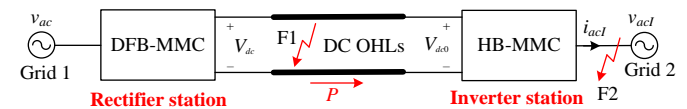


Fig. 3. HVDC link based on the proposed DFB-MMC.

Fig. 4 illustrates the equivalent circuit of the HVDC link shown in Fig. 3. During normal operation, the HB-MMC controls its DC terminal voltage at the rated value V_{dc0} and is thus represented by a DC voltage source V_{dc0} . To calculate the

steady state transmitted power, the DC transmission lines are simplified as a resistor R_{dc} in the equivalent circuit. The transmitted power of the inverter station is thus expressed as

$$P = V_{dc0} I_{dc} = V_{dc0} \frac{V_{dc} - V_{dc0}}{R_{dc}} = \frac{V_{dc0} V_{dc} - V_{dc0}^2}{R_{dc}} \quad (1)$$

where I_{dc} and V_{dc} are the DC current and voltage of the DFB-MMC, respectively.

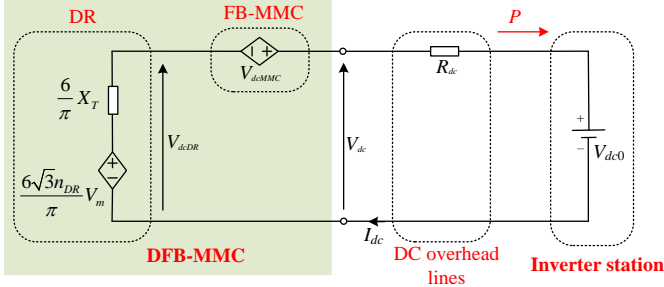


Fig. 4. Equivalent circuit of the HVDC link based on the proposed DFB-MMC.

Due to the series connection, the DC voltage of the DFB-MMC is the sum of the DR DC voltage V_{dcDR} and the FB-MMC DC voltage V_{dcMMC} :

$$V_{dc} = V_{dcDR} + V_{dcMMC} \quad (2)$$

Substituting (2) into (1), the active power P is rewritten as:

$$P = \frac{V_{dc0} (V_{dcDR} + V_{dcMMC}) - V_{dc0}^2}{R_{dc}} \quad (3)$$

The DC voltage produced by the DR is depicted as [12]:

$$V_{dcDR} = \frac{6}{\pi} (\sqrt{3} n_{DR} V_m - X_T I_{dc}) = \frac{6}{\pi} \left(\sqrt{3} n_{DR} V_m - X_T \frac{P}{V_{dc0}} \right) \quad (4)$$

where n_{DR} is the DR transformer ratio, X_T is the leakage reactance of the DR transformer, and V_m is the phase voltage amplitude of the AC grid. From (3) and (4), the active power P is rewritten as:

$$P = \frac{\pi V_{dc0}}{\pi R_{dc} + 6 X_T} V_{dcMMC} + \frac{6 \sqrt{3} n_{DR} V_m V_{dc0} - \pi V_{dc0}^2}{\pi R_{dc} + 6 X_T} \quad (5)$$

As depicted by (5), the transmitted power P of the HVDC link can be controlled by regulating the DC voltage V_{dcMMC} of the FB-MMC. The detailed design considering the relative power ratings of the DR and FB-MMC will be given in Section III.

C. Control Strategy

The control strategy of the proposed topology, including active power regulation and overvoltage alleviation during AC grid faults of the inverter station, is presented in this subsection.

1) Active power regulation

A simple power-DC voltage (P - V_{dc}) control scheme is proposed to regulate the DC voltage of the FB-MMC so as to control the transmitted power of the DFB-MMC according to (5).

As shown in Fig. 5 (a), the error between the power reference P^* and the measured actual power P of the DFB-MMC is fed to a PI control and its output sets the DC voltage reference V_{dcMMC}^* of the FB-MMC. To increase the power P of the DFB-MMC, the active power controller increases the output DC voltage V_{dcMMC} and, vice versa. The DC voltage of the FB-MMC is thus varied to follow the power order P^* . The active power P is

measured as the product of the DC voltage V_{dc} and DC current I_{dc} of the DFB-MMC and a low-pass filter (LPF) is used to take out the high-order harmonics of the DC power P .

As illustrated in Fig. 5 (b), the DC voltage reference V_{dcMMC}^* set by the active power controller is fed to the DC voltage control loop to regulate the d -axis current reference i_d^* , considering the sign of V_{dcMMC}^* . The current controller generates the required AC voltage v_c to be produced by the FB-MMC. The upper and lower arm voltage references are then generated considering the requirement from the circulating current controller, which are fed to the nearest level modulation (NLM) and SM capacitor voltage balancing control block to finally output the gating signals for the SMs.

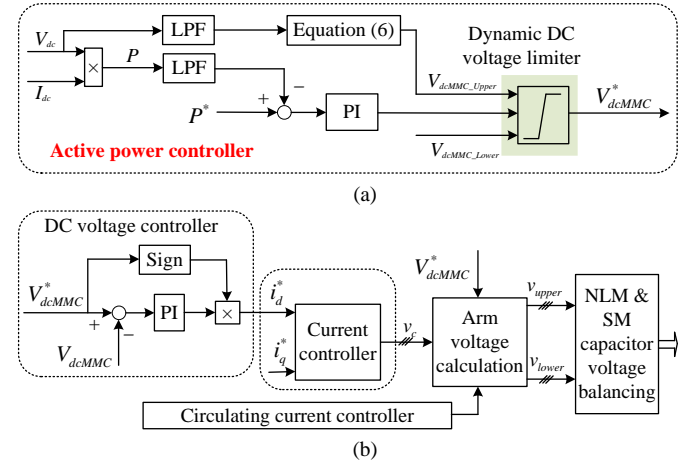


Fig. 5. Control strategy of the proposed DFB-MMC: (a) active power controller and (b) other control blocks.

2) Overvoltage alleviation during AC grid faults of inverter station

In the event of AC grid faults of the inverter station, the HB-MMC of the inverter station will operate in current limiting mode due to sudden drop of the AC grid voltage, and the active power output capability of the inverter significantly decreases. If the power transmitting from the rectifier station continues, the power unbalance between the rectifier and inverter stations can lead to overvoltage of the HVDC link.

To alleviate such overvoltage, a dynamic DC voltage limiter is proposed to enable the FB-MMC to generate negative DC voltage by limiting the output of the active power controller in the introduced P - V_{dc} control scheme, as illustrated in Fig. 5. The lower limit V_{dcMMC_Lower} is set at $-V_{dcMMC0}$ while the upper limit V_{dcMMC_Upper} is dependent on the DFB-MMC DC voltage V_{dc} , as described as

$$V_{dcMMC_upper} = \begin{cases} V_{dcMMC0}, & V_{dc} \leq V_{dc_thres} \\ V_{dc_thres} - V_{dc}, & V_{dc} > V_{dc_thres} \end{cases} \quad (6)$$

where V_{dcMMC0} is the rated DC voltage of the FB-MMC and V_{dc_thres} is the overvoltage threshold of the DFB-MMC and is set at $1.05 V_{dc0}$ in this paper. A low pass filter is used to take out the high-order harmonics of the DFB-MMC DC voltage V_{dc} in (6). During normal operation, V_{dc} is below is the overvoltage threshold V_{dc_thres} and the upper limit of the DC voltage reference V_{dcMMC_upper} is set at the rated DC voltage V_{dcMMC0} of the FB-MMC. In the event of AC grid faults of the inverter

station, the power transmission is interrupted and the active power PI controller saturates to try to increase the DC voltage to resume power transmission. Due to the power surplus, the DC voltage V_{dc} of the HVDC link increases and once V_{dc} exceeds the threshold V_{dc_thres} , the upper limit V_{dcMMC_upper} is limited to $V_{dc_thres} - V_{dc}$. Thus, the DC voltage reference V_{dcMMC}^* of the FB-MMC is set at $V_{dc_thres} - V_{dc}$ by the dynamic limiter and the FB-MMC outputs negative DC voltage to actively reduce the potential overvoltage of HVDC link. After fault isolation, the DC voltage of the HVDC link restores and the DC voltage reference V_{dcMMC}^* is set by the active power PI controller to automatically restore power transmission.

III. DESIGN CONSIDERATIONS OF THE PROPOSED TOPOLOGY

The design of the proposed hybrid HVDC converter is carried out in this section, considering the DC voltage and SM capacitance requirements of the FB-MMC.

A. DC Voltage Requirements of FB-MMCs

The DC voltage V_{dc} of the DFB-MMC is expressed as:

$$V_{dc} = V_{dc0} + R_{dc} I_{dc} = V_{dc0} + R_{dc} \frac{P}{V_{dc0}}. \quad (7)$$

From (4) and (7), the DC voltage of the FB-MMC is derived as

$$V_{dcMMC} = V_{dc} - V_{dcDR} = V_{dc0} + \left(R_{dc} + \frac{6}{\pi} X_T \right) \frac{P}{V_{dc0}} - \frac{6}{\pi} \sqrt{3} n_{DR} V_m. \quad (8)$$

With the variation of grid voltage, the DFB-MMC needs to be capable of regulating the transmitted power from zero to the rated value P_0 , by regulating the DC voltage V_{dcMMC} of the FB-MMC. The maximum DC voltage $V_{dcMMCmax}$ of the FB-MMC is required when the grid voltage V_m is at the lower limit of $V_{m0} - \Delta V_m$ while transmitting the rated power P_0 , where V_{m0} and ΔV_m are the rated value and variation of AC grid voltage V_m . From (8), $V_{dcMMCmax}$ is expressed as

$$V_{dcMMCmax} = V_{dc0} + \left(R_{dc} + \frac{6}{\pi} X_T \right) \frac{P_0}{V_{dc0}} - \frac{6}{\pi} \sqrt{3} n_{DR} (V_{m0} - \Delta V_m). \quad (9)$$

The required minimum DC voltage $V_{dcMMCmin}$ is defined when the grid voltage reaches the peak of $V_{m0} + \Delta V_m$ while the transmitted power P is zero, where the FB-MMC needs to output minimum voltage (negative) to suppress the transmitted power to zero. According to (8), $V_{dcMMCmin}$ is derived as

$$V_{dcMMCmin} = V_{dc0} - \frac{6\sqrt{3} n_{DR} (V_{m0} + \Delta V_m)}{\pi}. \quad (10)$$

To reduce the power rating of the FB-MMC, its negative voltage generating capability is utilized and thus the sum of the maximum and minimum voltages is zero:

$$V_{dcMMCmax} + V_{dcMMCmin} = 0. \quad (11)$$

From (9)-(11), the ratio n_{DR} of the DR transformer is governed by

$$n_{DR} = \frac{2\sqrt{3}\pi V_{dc0}^2 + \sqrt{3}(\pi R_{dc} + 6X_T)P_0}{36V_{dc0}V_{m0}}. \quad (12)$$

Setting the DR interface transformer ratio n_{DR} according to (12) ensures that the sum of the required maximum and minimum DC voltages of the FB-MMC is zero to minimize its power rating.

From (9), (10) and (12), the required maximum and minimum DC voltages of the FB-MMC are

$$V_{dcMMCmax} = -V_{dcMMCmin} = \frac{V_{dc0}}{V_{m0}} \Delta V_m + \frac{P_0}{V_{dc0}} \left(\frac{3X_T}{\pi} + \frac{R_{dc}}{2} \right) \left(1 + \frac{\Delta V_m}{V_{m0}} \right) \quad (13)$$

The rated DC voltage of the FB-MMC is designed to ensure the maximum and minimum DC voltages as depicted by (13) can be met, considering 10% overrating, as

$$V_{dcMMC0} = 1.1V_{dcMMCmax} = -1.1V_{dcMMCmin}. \quad (14)$$

From (13) and (14), the ratio between the rated FB-MMC DC voltage and the rated DFB-MMC DC voltage (i.e. V_{dcMMC0}/V_{dc0}) is shown in Fig. 6. The ratio V_{dcMMC0}/V_{dc0} is directly proportional to the AC grid voltage variation of $\Delta V_m/V_{m0}$ and is 9.3%, 12.7% and 15% respectively when $\Delta V_m/V_{m0}$ is equal to 5%, 8% and 10%. This indicates the power rating of the FB-MMC is dependent on the grid variation and is 15% of that of the DFB-MMC (i.e. 15% P_0) when 10% grid voltage variation (i.e. $\Delta V_m/V_{m0}=10\%$) is considered. Thus, only low power rating of the FB-MMC is required for the proposed topology while the majority power is transmitted via the cost-effective and efficient diode rectifier. Different to the FB-MMC DC voltage V_{dcMMC0} , the transformer ratio n_{DR} is independent on the grid variation ΔV_m , as depicted by (12).

Considering the relatively lower current rating of IGBTs (adopted in the FB-MMC) than that of diodes (adopted in the DR), parallel connection of IGBTs as commonly used in HB-MMC systems [24, 25] can be adopted to increase the overall current capacity of the FB-MMC to match that of the diodes.

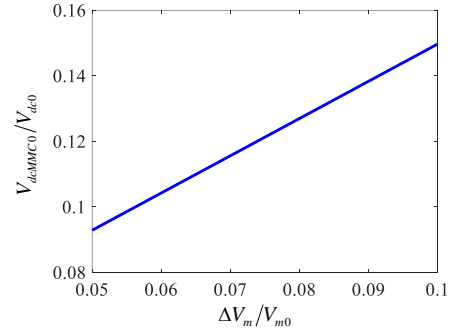


Fig. 6. Ratio between the rated FB-MMC DC voltage and the rated DFB-MMC DC voltage (i.e. V_{dcMMC0}/V_{dc0}) with the variation of AC grid voltage.

B. SM Capacitance Requirements

Different from conventional FB-MMC, the SM capacitor voltage variation of the FB-MMC in the proposed arrangement largely depends on the AC grid voltage variation and thus the required SM capacitance is presented in this subsection.

The arm voltage of the proposed DFB-MMC is expressed as

$$v_{arm} = \frac{1}{2} V_{dcMMC} - n_{MMC} (V_{m0} + \Delta V_m) \sin(\omega t) \quad (15)$$

where n_{MMC} is the FB-MMC interface transformer ratio and ω is the angular frequency of the AC grid. Assuming the converter is lossless, the AC power of the FB-MMC equals its DC power:

$$\frac{3}{2} n_{MMC} I_{mMMC} (V_{m0} + \Delta V_m) = \frac{P}{V_{dc0}} V_{dcMMC} \quad (16)$$

where I_{mMMC} is the converter-side peak current of the FB-MMC. From (16), I_{mMMC} is obtained as

$$I_{mMMC} = \frac{2V_{dcMMC}P}{3n_{MMC}V_{dc0}(V_{m0} + \Delta V_m)}. \quad (17)$$

According to (17), the arm current is derived as

$$i_{arm} = \frac{P}{3V_{dc0}} + \frac{V_{dcMMC}P}{3n_{MMC}V_{dc0}(V_{m0} + \Delta V_m)} \sin(\omega t - \varphi) \quad (18)$$

where φ is the phase angle. From (15) and (18), integrating the product of the arm voltage and current yields the arm energy variations as

$$\begin{aligned} \Delta E_{arm}(\omega t) &= \frac{1}{\omega} \int_0^{\omega t} v_{arm} i_{arm} d(\omega t) \\ &= -\frac{V_{dcMMC}^2 P}{6n_{MMC}V_{dc0}\omega(V_{m0} + \Delta V_m)} [\cos(\omega t - \varphi) - \cos \varphi] + \\ &\quad \frac{P(V_{m0} + \Delta V_m)}{3\omega V_{dc0}} [\cos(\omega t) - 1] + \\ &\quad \frac{V_{dcMMC}P}{12n_{MMC}V_{dc0}\omega} [\sin(2\omega t - \varphi) + \sin \varphi] \end{aligned} \quad (19)$$

As depicted by (19), the arm energy variation peaks depend on the transmitted power P and the grid voltage variation ratio $\Delta V_m/V_{m0}$, as shown in Fig. 7. When the grid voltage decreases to 0.9 pu (i.e. $1+\Delta V_m/V_{m0}=0.9$) while transmitting the rated power, the arm energy variation peak of the tested system reaches the maximum value of 320 kJ, which defines the required SM capacitance. The corresponding SM capacitance requirement is 31 kJ/MVA, which is in agreement with the guidance value of 30~40 kJ/MVA as suggested by ABB in [26].

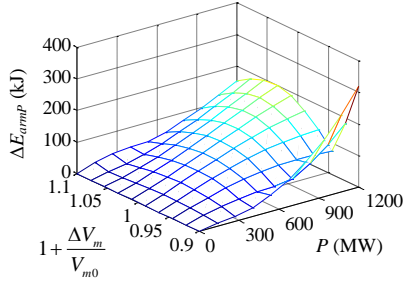


Fig. 7. Arm energy variation peak of the proposed converter with the variation of grid voltage $1+\Delta V_m/V_{m0}$ and transmitted power P .

During normal operation, the grid voltage (i.e. $1+\Delta V_m/V_{m0}$ in Fig. 7) is usually in the range of 0.95~1.05 and the arm energy variation peak is less than the designed value of 320 kJ. Thus, with the same SM capacitor voltage variation, the SMs of the proposed topology can be switched less frequently than that of conventional MMCs [27], leading to reduced switching losses.

C. Comparison between the Proposed DFB-MMC and Other Alternatives

The overall loss of the conventional HB-MMC station is typically 0.8% [28], including semiconductor valves, transformers, valve reactors, DC reactors, and auxiliary supplies, etc. The power losses of the semiconductor valves are around half of the overall loss of the station, i.e. 0.4% [29, 30]. The switching and conduction losses of the conventional HB-MMC are 30% and 70% of the semiconductor valve power losses, respectively. The FB-MMC has similar switching losses to that of the HB-MMC but its conduction losses are doubled. The loss of the FB-MMC is thus derived as 1.08% [3, 28, 29, 31]. Considering the DR loss of 0.5% [16, 32] and the FB-MMC power rating of $0.15P_0$, the loss of the proposed DFB-

MMC in nominal condition is calculated as $1.08\% \times 0.15 + 0.5\% \times 0.85 = 0.59\%$, being 26.6% lower than that of the conventional HB-MMC (i.e. 0.8%).

The power losses of the semiconductor valves consist of switching and conduction losses and their ratio varies in the range of 20%/80% and 40%/60%, depending on the adopted IGBT technology and the modulation strategy. Considering the ratio of 20%/80%, the loss of the proposed DFB-MMC is 25.9% lower than that of the conventional HB-MMC. Similarly, the loss is reduced by 27.4% when the ratio between switching and conduction losses is 40%/60%. It should be noted that the ratio between the losses of HVDC stations and the transmitted power is not constant and changes with the variation of the transmitted power and network condition. The aforementioned losses are obtained when transmitting the rated power, while for other power levels, the losses will vary [3, 28, 29, 31].

The major power is transferred through the DR in the proposed topology and only low power rating FB-MMC is required (i.e. maximum 15% of the system power rating as shown in Fig. 6). Thus, the cost of the proposed converter is substantially reduced compared to the conventional MMC, considering high efficiency of the DR. In addition, the capitalized cost associated with losses is typically in the range of 3000~5000 €/kW [29, 30, 33, 34] and, considering the average value of 4000 €/kW and 26.6% loss reduction of the proposed topology, the cost is further reduced by 10 M€ if the conventional MMC rated at 1200 MW is replaced by the proposed DFB-MMC.

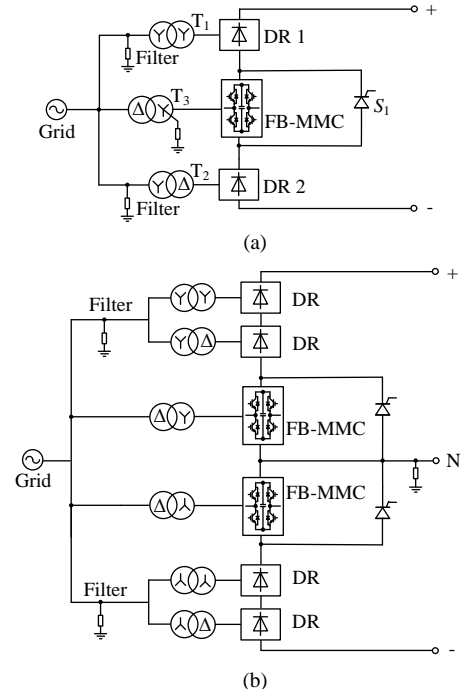


Fig. 8. Possible system configurations based on the proposed converter: (a) symmetrical monopole and (b) bipole.

Compared to conventional line-commutated converters (LCCs), the size of filters required by the DR in the proposed topology is reduced, leading to lower volume and cost [12, 35, 36]. In addition, the FB-MMC can actively compensate reactive power and suppress harmonics generated by the DR [14], which

further reduces the filter size of the proposed converter. Moreover, the power loss of the proposed DFB-MMC is comparable to that of the LCC rectifier (0.59% vs. 0.63% for LCC [28, 31]).

D. System Configuration

This subsection provides high-level discussions of possible system configurations based on the proposed DFB-MMC, as shown in Fig. 8.

Fig. 8 (a) depicts the schematic diagram of the generic symmetrical monopole configuration. Two diode rectifiers are connected to the positive and negative DC poles, respectively, with the FB-MMC connected in series in the middle. A Δ/Y transformer with converter-side high impedance grounding is taken as an example [37-39].

Fig. 8 (b) display a generic representation of the bipole configuration with metallic return. In the event of one pole outage, the healthy pole can continue operating with the neutral line, similar to conventional MMC based bipole HVDC system arrangement.

is also applicable to cable schemes. To improve the simulation accuracy, each OHL is modeled as 10 pi sections with detailed parameters listed in Table I [42, 43]. The proposed DFB-MMC is adopted as the rectifier station and operates on power control mode, whilst the HB-MMC of the inverter station controls its DC terminal voltage constant [3]. The FB-MMC and HB-MMC are represented by detailed submodule-based switching function model [44] while the DR is represented by detailed switching model. The parameters of the tested DFB-MMC are listed in Table I. The ACCB is modelled with an opening delay time of 60 ms and can only be opened at current zero crossing. DC reactors of 50 mH are connected at the DC terminals of the proposed converter to limit the fault current rising rate, which is similar to the conventional HB-MMC based systems [22, 41].

A. Normal Operation

Two worst scenarios, i.e. the grid voltage of 0.9 and 1.1 pu, are considered in this subsection to test the power regulation capability of the proposed HVDC converter.

1) Low grid voltage of 0.9 pu

Initially, the grid voltage is at the lower limit and the power order of the rectifier station is set at zero. The output voltage of the FB-MMC is zero and the DR is reversely blocked due to the low AC grid voltage, leading to zero transmitted power of the DFB-MMC, as seen in Fig. 9 (b), (d) and (f). The DC voltage of DFB-MMC is controlled at the rated value of 1100 kV, Fig. 9 (g).

At $t=0.5$ s, the power reference of the DFB-MMC is ramped up from 0 to 1 pu. Thus, the DC voltage of the FB-MMC starts to increase, as shown in Fig. 9 (f). At $t=0.56$ s, the DR starts to conduct and its AC currents increase for power transmission while the DR DC voltage decreases due to the voltage drop across the leakage reactance of the DR transformer, seen in Fig. 9 (b), (c), (d), (e) and (i). At around $t=0.8$ s, the DC voltage of the FB-MMC increases to 148 kV and the transmitted power reaches the rated value of 1200 MW with the grid voltage at the lower limit of 0.9 pu, as observed in Fig. 9 (a), (d) and (f).

2) High grid voltage of 1.1 pu

In this scenario, the grid voltage is at the upper limit and the power reference of the DFB-MMC is initially set at the rated value. Due to the high AC grid voltage, the power transmitted via the DR is over the DFB-MMC rated power of 1200 MW, seen in Fig. 10 (b). Thus, the FB-MMC outputs negative voltage and operates on inverter mode to export power from the HVDC link to the AC grid and control the DFB-MMC power at the rated, as displayed in Fig. 10 (c), (d) and (f). In such condition, part of the power circulates between the FB-MMC and the diode rectifier, leading to additional losses. However, the circulation power is only a small portion of the total transmitted power (53 MW/1200 MW=4.4%, as shown in Fig. 10 (c) and (d)) so does not compromise the efficiency of the entire system.

At $t=0.5$ s, the power reference of the DFB-MMC is ramped down to 0 in 0.2 s. The DC voltage of the FB-MMC starts to decrease, which leads to the increase of the DR DC voltage, considering the nearly constant HVDC link voltage controlled by the inverter station, as shown in Fig. 10 (e), (f) and (g). The transmitted power of the DR is thus reduced, Fig. 10 (b) and (i).

At around $t=0.75$ s, the DC voltage of the FB-MMC

TABLE I
Nominal parameters of the tested system.

PARAMETER		NOMINAL VALUE
Grid	Voltage	400 kV
	Short circuit level	10 GW
	X/R ratio	14
Power rating P_0		1200 MW
Overall DC voltage		± 550 kV
FB-MMC	DC-link voltage V_{dcMMC0}	165 kV
	Power rating	180 MW
	SM number per arm	80
	SM capacitor voltage	2.06 kV
	SM capacitance	5.4 mF
	Arm inductance	0.1 pu
	Grid- and converter-side voltages of transformer	400 kV/84 kV
	Transformer leakage inductance	0.15 pu
12-pulse diode rectifier	Grid- and converter-side voltages of transformer	400 kV/422 kV
	Transformer leakage inductance	0.15 pu
DC overhead line	Length	150 km
	R , L and C of DC OHLs [40]	10 m Ω /km, 0.9 mH/km, 0.02 μ F/km

IV. SIMULATION RESULTS

The proposed topology and control scheme are assessed using the HVDC link shown in Fig. 3 in Matlab/Simulink environment, considering normal operation and faults. The symmetrical monopole configuration as illustrated in Fig. 8 (a) is adopted, where the DC voltage and the length of the overhead lines (OHLs) are ± 550 kV and 150 km, respectively. These are comparable to the DC voltage of ± 500 kV in the Zhangbei four-terminal HVDC project with OHLs of 66 km, 126 km, 219 km and 227 km [41]. In addition to OHLs, the proposed converter

decreases to around -148 kV and the DR becomes reverse blocked. The transmitted power of the DFB-MMC is thus reduced to zero even with the grid voltage at the upper limit of 1.1 pu, as observed in Fig. 10 (a), (b), (d) and (f).

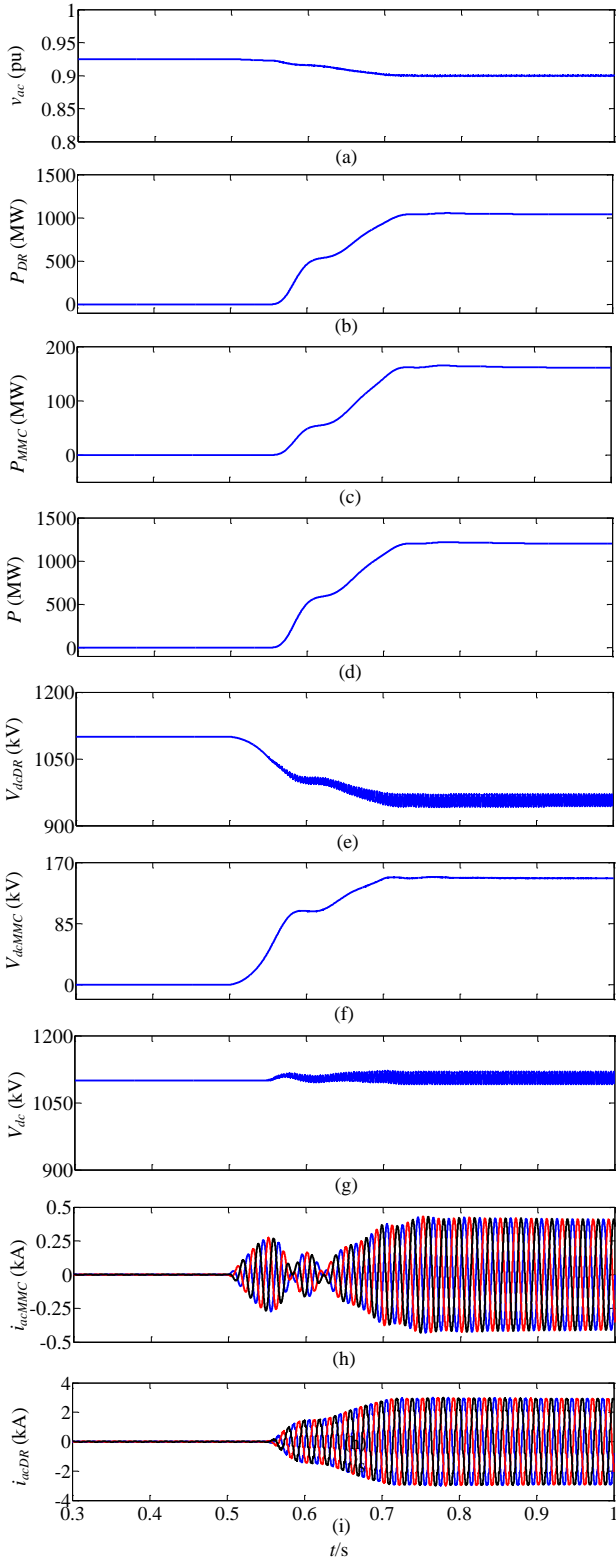


Fig. 9. Waveforms during normal operation with low grid voltage (0.9 pu): (a) grid voltage v_{ac} , (b) DR DC power P_{DR} , (c) FB-MMC DC power P_{MMC} , (d) DFB-MMC DC power P , (e) DR DC voltage V_{dcDR} , (f) FB-MMC DC voltage V_{dcMMC} , (g) DFB-MMC DC voltage V_{dc} , (h) FB-MMC AC currents i_{acMMC} and (i) DR AC currents i_{acDR} .

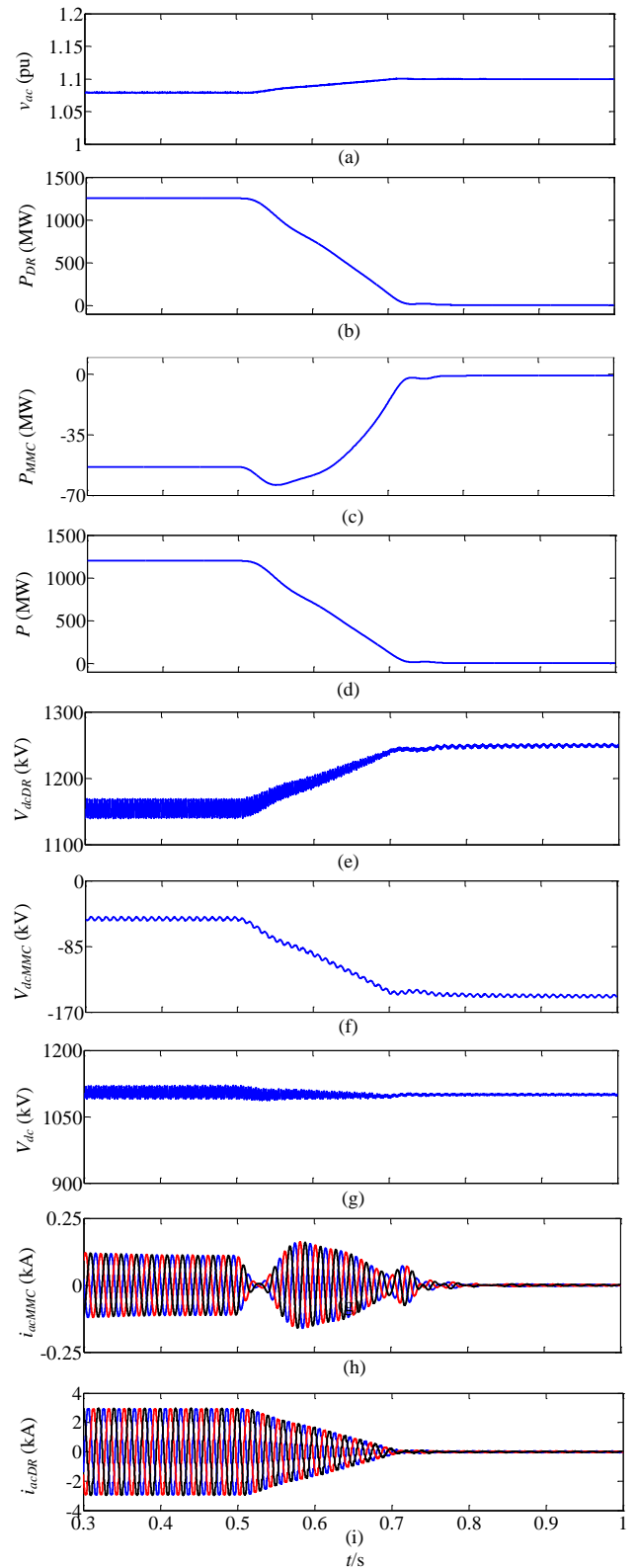


Fig. 10. Waveforms during normal operation with high grid voltage (1.1 pu): (a) grid voltage v_{ac} , (b) DR DC power P_{DR} , (c) FB-MMC DC power P_{MMC} , (d) DFB-MMC DC power P , (e) DR DC voltage V_{dcDR} , (f) FB-MMC DC voltage V_{dcMMC} , (g) DFB-MMC DC voltage V_{dc} , (h) FB-MMC AC currents i_{acMMC} and (i) DR AC currents i_{acDR} .

With the variation of the grid voltage in the range 0.9~1.1 pu, the proposed DFB-MMC is capable of regulating the transmitted power from zero to the rated power, benefiting from

the variable DC voltage operating capability of the FB-MMC.

B. DC Faults

In this scenario, a pole-to-pole permanent DC fault F1 is applied at the middle of the DC OHLs at $t=1$ s, as illustrated in Fig. 3.

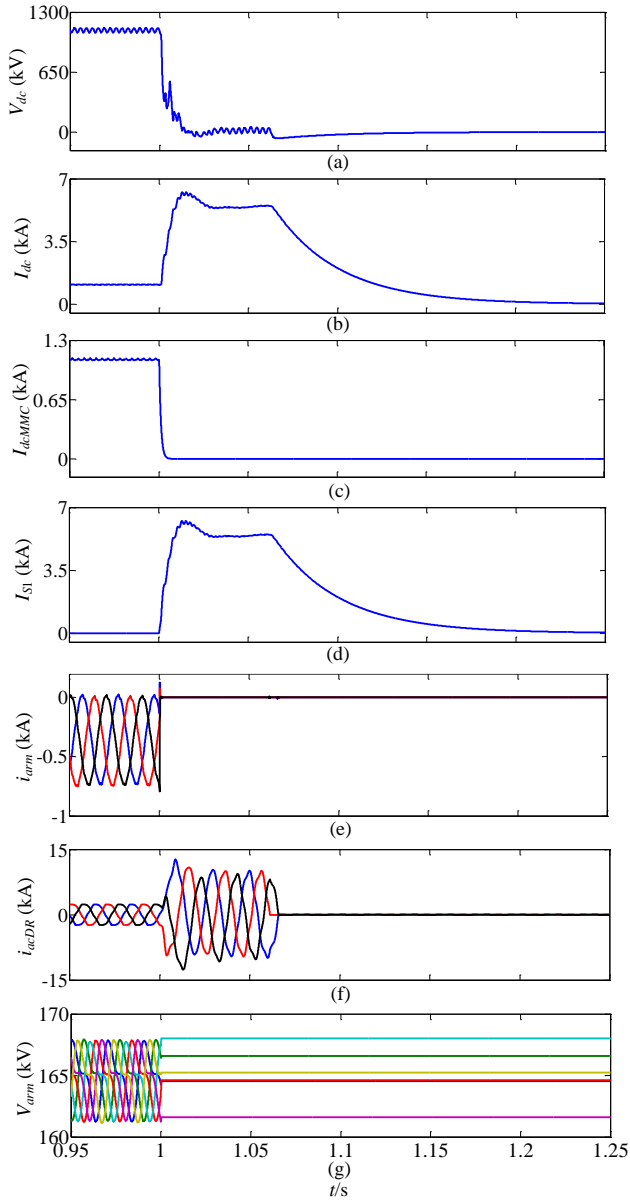


Fig. 11. Waveforms during the DC fault F1: (a) DC voltage V_{dc} , (b) DC current I_{dc} , (c) FB-MMC DC current I_{dcMMC} , (d) thyristor current I_{S1} , (e) FB-MMC arm currents i_{arm} , (f) DR AC currents i_{acDR} and (g) sum of SM capacitor voltages in each arm of the FB-MMC.

After fault occurrence, the DC voltage of the HVDC link drops to around zero as shown in Fig. 11 (a) and the DFB-MMC is blocked once the fault is detected, while the thyristor valve S_1 is switched on with 200 μ s delay time. The DC current flowing through the FB-MMC is quickly suppressed to zero following the blocking of the station, as seen in Fig. 11 (c). The fault current from the AC grid through the DR thus only flows through the thyristor valve S_1 and feeds the fault, as displayed in Fig. 11 (b), (d) and (f). The currents flowing through the

converter arms of the FB-MMC are also zero and the FB SMs are not subject to additional thermal stress during DC faults, as seen in Fig. 11 (e). The FB-MMC is effectively bypassed by the thyristor valve S_1 and thus the capacitor voltages of the FB SMs do not have over charging issue, as demonstrated in Fig. 11 (g).

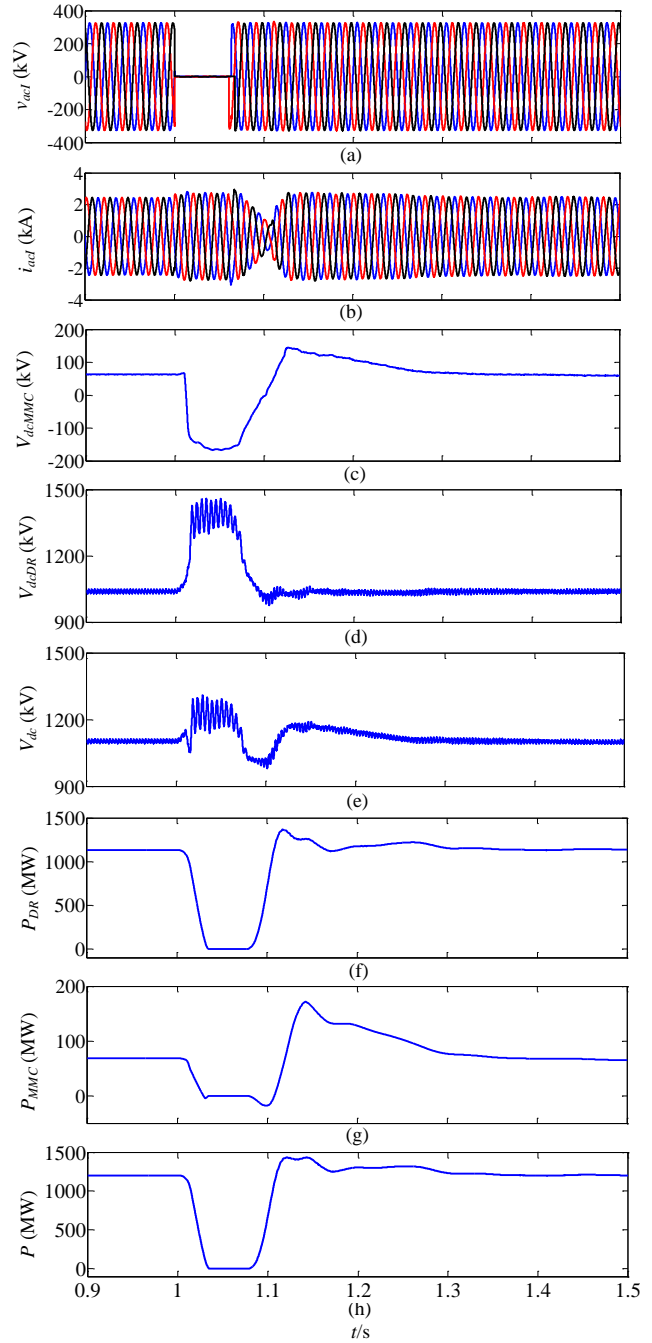


Fig. 12. Waveforms during the AC fault F2 at the AC grid of the inverter station: (a) inverter station AC voltages v_{ac1} , (b) inverter station AC currents i_{ac1} , (c) FB-MMC DC voltage V_{dcMMC} , (d) DR DC voltage V_{dcDR} , (e) DFB-MMC DC voltage V_{dc} , (f) DR DC power P_{DR} , (g) FB-MMC DC power P_{MMC} and (h) DFB-MMC DC power P .

At $t=1.061$ s, the AC circuit breaker on the DFB-MMC AC side opens and the AC currents flowing through the DR drop to zero, seen in Fig. 11 (f). As observed in Fig. 11 (b) and (d), the fault currents on DC side gradually decay, depending on the resistance and inductance of the fault current path. As shown in

Fig. 11 (d), the peak fault current flowing through the thyristor valve S_1 is around 6.2 kA and is in the safe operation range of typical high power thyristors [45, 46]. It is equivalent to 5.7 pu (6.2 kA/1.09 kA), which is in the similar range to that in [47, 48].

C. Inverter Station AC Faults

To test the proposed topology and control in the event of an AC grid fault of the inverter station, a symmetrical solid fault F2 is applied at the AC side of the HB-MMC of the inverter station as illustrated in Fig. 3 at $t=1$ s and is cleared after 60 ms.

As shown in Fig. 12 (a) and (b), the grid voltage of the inverter station drops to zero after fault occurrence and the inverter HB-MMC operates on current limiting mode to support the AC grid. As the output power of the HB-MMC is reduced to zero and the rectifier station DFB-MMC still imports energy to HVDC-link, the DC voltage increases. Once the DC voltage reaches 1.05 pu, the proposed dynamic DC voltage limiter is activated to actively reduce the DC voltage of the FB-MMC and the transmitted power is quickly suppressed to zero, as displayed in Fig. 12 (c), (f), (g) and (h). This effectively reduces the DC overvoltage of the HVDC link, as shown in Fig. 12 (e).

After fault clearance $t=1.06$ s, the power transmission of the inverter HB-MMC resumes and the system autonomously restores normal operation without communication.

V. CONCLUSION

A unidirectional hybrid HVDC converter composed of diode rectifier and FB-MMC is proposed, where the FB-MMC operates with variable DC voltage to regulate the transmitted power. The thyristor connected at the DC terminal of the FB-MMC is switched on during DC faults to bypass the FB-MMC so as to avoid overcharge of the FB SMs. The major power is transferred through the DR and only low power rating FB-MMC is required. Compared to the conventional MMC, the losses of the proposed converter are reduced by around 20%. The proposed active power controller regulates the DC voltage of the FB-MMC to control the transmitted power. The FB-MMC increases the output DC voltage to increase the transmitted power and, vice versa. During AC grid faults of the inverter station, the FB-MMC outputs negative DC voltage with the proposed dynamic DC voltage limiter to effectively alleviate overvoltage of the HVDC link. The proposed topology achieves good balance between efficiency and controllability and provides a promising solution for the bulk energy transmission.

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