

# *R*-matrix electron-impact excitation data for the B-like iso-electronic sequence<sup>★</sup>

G. Y. Liang<sup>1</sup>, N. R. Badnell<sup>2</sup>, and G. Zhao<sup>1</sup>

<sup>1</sup> National Astronomical Observatories, CAS, 100012 Beijing, PR China

<sup>2</sup> Department of Physics, University of Strathclyde, Glasgow, G4 0NG, UK  
e-mail: gyl.liang@bao.ac.cn

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## ABSTRACT

We have carried-out parallel intermediate-coupling frame transformation *R*-matrix calculations for electron-impact excitation amongst the 204 close-coupling levels of the  $2s^x 2p^y$  ( $x + y = 3$ ),  $2s^2\{3, 4\}l$ ,  $2s2p\{3, 4\}l$ , and  $2p^2 3l$  configurations for all boron-like ions from  $C^+$  to  $Kr^{31+}$ . We have also included the configuration interaction due to the  $2p^2 4l$ ,  $2s3l/$  and  $2p3s3l$  configurations. A detailed comparison has been made of the target structure and excitation data for four specific ions (viz.,  $Ne^{5+}$ ,  $Ar^{13+}$ ,  $Fe^{21+}$  and  $Kr^{31+}$ ) that span the sequence, so as to assess the accuracy over the entire sequence. Effective collision strengths ( $\Upsilon$ 's) are presented at temperatures ranging from  $2 \times 10^2(z + 1)^2$  K to  $2 \times 10^6(z + 1)^2$  K (where  $z$  is the residual charge of the ions, i.e.  $Z - 5$ ). Detailed comparisons for the (effective) collision strengths ( $\Upsilon$ 's)  $\Omega$  are made with the results of previous calculations for the four representative ions. Furthermore, we examine the iso-electronic trends of the effective collision strengths as a function of temperature.

**Key words.** atomic data – atomic processes – plasmas

## 1. Introduction

Emission lines of boron-like ions have been recorded in both earlier spacecraft (Malinovsky & Heroux 1973; Huber et al. 1973; Acton et al. 1985) and more recent Hinode/EIS (Brown et al. 2008; Landi & Young 2009; Del Zanna 2012) solar observations. The diagnostic usefulness of B-like  $n = 2 \rightarrow n = 2$  transition lines was first noted by Flower & Nussbaumer (1973) for several ions, viz. sodium, silicon, and sulphur. Later, Peng & Pradhan (1995) performed a systematic investigation for line intensity ratios of the boron-like iso-electronic sequence (including C II, N III, O IV, Ne VI, Mg VIII, Al IX, Si X, and S XII), and illustrated some line ratios that are sensitive to electron temperature or electron density. The authors used data from an *R*-matrix calculation by Zhang et al. (1994), which included just the  $n = 2$  configurations. However, Keenan et al. (2000, 2002) noticed a slight error by Zhang et al. (1994) when including term coupling coefficients in their *R*-matrix calculation. Keenan et al. (2002) re-calculated the excitation data amongst the fine-structure levels of the  $n = 2$  configurations for Si X and S XII. The diagnostic line ratios involving those levels were re-examined by them also and applied to solar observations. Liang & Zhao (2008) furthermore applied the electron density diagnostic line ratio of two  $3d-2p$  transition lines to stellar observations. However, the available excitation data for  $n = 2 \rightarrow n = 3$  transitions in the boron-like iso-electronic sequence are mainly from distorted-wave (DW) calculations, which omit the contribution from resonances. In addition to the resonances attached to them, more highly excited states also contribute to lower-lying line ratios

via cascades – see for example Del Zanna et al. (2012) and Foster et al. (2012), where *R*-matrix data were additionally supplemented by DW calculations.

For the astrophysically important  $Fe^{21+}$  ion, Badnell et al. (2001) performed a 204-level intermediate-coupling frame transformation (ICFT) *R*-matrix calculation, which included a much larger configuration interaction (CI) expansion. Recently, Liang et al. (2009a, 2011) extended *R*-matrix calculations up to  $n = 3$  and 4 for  $Si^{9+}$  and  $S^{11+}$  ions, respectively. Ludlow et al. (2010) performed Breit-Pauli *R*-matrix calculations for all ions of the argon isonuclear sequence. The boron-like case used a close-coupling expansion comprising the  $2s^x 2p^y$  ( $x + y = 3$ ),  $2s^2\{3, 4, 5\}l$  configurations. For other ions along this iso-electronic sequence, the distorted-wave calculations performed by Zhang & Sampson (1994a,b) are still the main source of data for various modelling databases, e.g. Chianti v7 (Landi et al. 2012), AtomDB v2<sup>1</sup>.

Here, we report on calculations for the electron-impact excitation of the boron-like iso-electronic sequence from  $C^+$  to  $Kr^{31+}$  ions that were made using the ICFT *R*-matrix method. This paper is part of our series of works on iso-electronic sequences: Li-like, Liang et al. (2011); F-like, Witthoef et al. (2007); Ne-like, Liang & Badnell (2010); and Na-like, Liang et al. (2009a,b). This work is part of the UK Atomic Processes for Astrophysical Plasmas (APAP) network<sup>2</sup>.

The remainder of this paper is organized as follows. In Sect. 2, we discuss details of the calculational method and pay particular attention to comparing our underlying atomic structure results with those of previous workers. The model for the scattering calculation is outlined in Sect. 3. The excitation results themselves are discussed in Sect. 4.

<sup>★</sup> These data are made available in the archives of APAP via <http://www.apap-network.org>, OPEN-ADAS via <http://open.adas.ac.uk> as well as at the CDS via an anonymous ftp to [cdsarc.u-strasbg.fr](http://cdsarc.u-strasbg.fr) (130.79.128.5) or via <http://cdsarc.u-strasbg.fr/viz-bin/qcat?J/A+A/547/A87>

<sup>1</sup> <http://www.atomdb.org/>

<sup>2</sup> <http://www.apap-network.org>

**Table 1.** Thomas-Fermi potential scaling factors used in our AUTOSTRUCTURE calculations (see text for details).

Ion	1s	2s	2p	3s	3p	3d	4s	4p	4d	4f
C	1.42633	1.25671	1.19952	1.58317	1.33938	1.25491	1.47430	1.50168	1.41676	1.87478
N	1.42754	1.29142	1.18509	1.55209	1.33194	1.38132	1.53577	1.17635	1.55789	1.95182
O	1.41103	1.24220	1.17671	1.64434	1.34306	1.41337	1.68623	1.29607	1.48413	2.30820
F	1.40597	1.24278	1.17399	1.64015	1.34575	1.43378	1.54779	1.33411	1.48348	2.31452
Ne	1.40173	1.24350	1.17260	1.63435	1.34871	1.44626	1.72622	1.36416	1.52383	3.15127
Na	1.39840	1.24440	1.17205	1.62817	1.35159	1.45478	1.27730	1.54966	1.50999	0.58666
Mg	1.39554	1.24527	1.17189	1.62232	1.35422	1.46091	1.38464	1.31611	1.53481	0.57992
Al	1.39331	1.24606	1.17194	1.61707	1.35664	1.46554	1.44070	1.35498	1.51784	1.12328
Si	1.39126	1.24678	1.17212	1.61234	1.35881	1.46915	1.45299	1.35280	1.53085	1.22926
P	1.38951	1.24743	1.17236	1.60821	1.36083	1.47206	1.46557	1.35802	1.51540	1.33250
Cl	1.38654	1.24854	1.17292	1.60085	1.36417	1.47653	1.47955	1.36821	1.53241	1.44182
Ar	1.38536	1.24902	1.17321	1.59800	1.36562	1.47826	1.48396	1.37121	1.53345	1.47479
K	1.38433	1.24945	1.17349	1.59525	1.36693	1.47974	1.48780	1.37360	1.53422	1.49809
Ca	1.38338	1.24985	1.17377	1.59276	1.36813	1.48103	1.49080	1.37569	1.53488	1.51727
Sc	1.38253	1.25020	1.17403	1.59051	1.36923	1.48216	1.49331	1.37751	1.53545	1.53287
Ti	1.38177	1.25053	1.17428	1.58845	1.37023	1.48318	1.49540	1.37914	1.53595	1.54423
V	1.38108	1.25084	1.17452	1.58660	1.37117	1.48410	1.49729	1.38049	1.53639	1.55359
Cr	1.38045	1.25112	1.17474	1.58487	1.37202	1.48491	1.49872	1.38181	1.53632	1.56402
Mn	1.37987	1.25137	1.17495	1.58327	1.37281	1.48564	1.50016	1.38294	1.53668	1.57186
Fe	1.37933	1.25161	1.17515	1.58174	1.37353	1.48629	1.50142	1.38397	1.53745	1.57746
Co	1.37884	1.25183	1.17534	1.58037	1.37421	1.48690	1.50278	1.38487	1.53772	1.58350
Ni	1.37839	1.25204	1.17552	1.57908	1.37485	1.48746	1.50382	1.38573	1.53800	1.58859
Cu	1.37797	1.25223	1.17570	1.57796	1.37542	1.48796	1.50475	1.38649	1.53824	1.59381
Zn	1.37758	1.25242	1.17586	1.57685	1.37597	1.48843	1.50560	1.38722	1.53845	1.59748
Ga	1.37721	1.25259	1.17601	1.57582	1.37649	1.48887	1.50638	1.38789	1.53866	1.60106
Ge	1.37687	1.25275	1.17616	1.57485	1.37703	1.48933	1.50708	1.38854	1.53885	1.60483
As	1.37655	1.25290	1.17630	1.57395	1.37749	1.48971	1.50774	1.38913	1.53902	1.60791
Se	1.37625	1.25305	1.17643	1.57306	1.37789	1.49002	1.50837	1.38965	1.53918	1.61027
Br	1.37597	1.25318	1.17656	1.57226	1.37829	1.49035	1.50894	1.39015	1.53934	1.61280
Kr	1.37570	1.25330	1.17668	1.57152	1.37868	1.49067	1.50946	1.39063	1.53948	1.61537

## 2. Sequence calculation

The aim of this work is to perform *R*-matrix calculations employing the ICFT method (see Griffin et al. 1998) for all boron-like ions from  $C^+$  to  $Kr^{31+}$ . The close-coupling (CC) expansion we used consists of the  $2s^x 2p^y$  ( $x + y = 3$ ),  $2s^2\{3, 4\}l$ ,  $2s2p\{3, 4\}l$ , and  $2p^2 3l$  (92 LS terms, 204 fine-structure levels) configurations. The additional configuration interaction (CI) from the  $2p^2 4l$ ,  $2s3l3l'$  and  $2p3s3l$  (71 LS terms, 160 fine-structure levels) configurations was included for the target structure used in the collision calculation.

### 2.1. Structure: level energies

The target wavefunctions (1s–4f) were obtained from AUTOSTRUCTURE (AS, Badnell 1986) using the Thomas-Fermi-Dirac-Amaldi model potential. Relativistic effects were included perturbatively from the one-body Breit-Pauli operator (viz. mass-velocity, spin-orbit and Darwin) without valence-electron two-body fine-structure operators. This is consistent with the operators included in the standard Breit-Pauli *R*-matrix suite of codes. The radial scaling parameters,  $\lambda_{nl}$  ( $n = 1-4$ ;  $l \in s, p, d$ , and  $f$ ), were obtained separately for each ion by a three-step optimization procedure. In the first step, the weighted sum of all term energies of the  $1s^2 2s^x 2p^y$  ( $x + y = 3$ ) configurations was minimized by varying the  $\lambda_{1s}$ ,  $\lambda_{2s}$  and  $\lambda_{2p}$  scaling parameters. Then, the energies of the  $1s^2 2s^2 3l$  and  $1s^2 2s^2 4l$  configurations were minimized by varying the  $\lambda_{3l}$  and  $\lambda_{4l}$  scaling parameters, respectively. The resultant scaling parameters are listed in Table 1. For lower charged ions,  $\lambda_{4f}$  is far away from unity. Tests show that it is insensitive to optimization and the atomic structure itself is insensitive to it.

A comparison of level energies is made with the experimentally derived data available from the compilation of NIST v4<sup>3</sup>, and with other theoretical results, for four specific ions ( $Ne^{5+}$ ,  $Ar^{13+}$ ,  $Fe^{21+}$ , and  $Kr^{31+}$ ) that span the sequence, so as to assess the accuracy of our present structure over the entire iso-electronic sequence – see Tables 2–5. For many excited levels of the  $n = 3$  and 4 complexes, the present AS calculation agrees to better than within 1% with the NIST v4<sup>3</sup> recommended values for the four ions. For levels of  $n = 2$  configurations, the energy difference is less than 4%. For highly charged ions, this discrepancy becomes smaller. Therefore, we performed a calculation with level energy corrections to the diagonal of the Hamiltonian matrix before diagonalization for the 15 fine-structure levels of the  $n = 2$  configurations of almost all ions over the iso-electronic sequence (except for  $Z = 29-35$ ) and iterated to convergence. For those levels missing in the NIST compilation, we adopted the mean value of differences between our level energies and corresponding NIST values of the same configuration. The resulting *e*-vectors and *e*-energies were used to calculate the oscillator strengths and archived energies.

For  $Ne^{5+}$ , Mitnik et al. (2001) performed a multi-configuration Hartree-Fock (MCHF) calculation with three pseudo-orbitals ( $\bar{5}s$ ,  $\bar{5}p$ , and  $\bar{5}d$ ) included, which shows a better agreement with NIST v4 data for the levels of  $n = 2$  configurations, see Table 2. For higher excited levels of  $n = 3$  and 4 configurations, the two different sets of predictions agree better, to within 1%.

For  $Ar^{13+}$ , a GRASP calculation is available, which included the  $2s^x 2p^y$  ( $x + y = 3$ ),  $2s^2\{3, 4, 5\}l$ ,  $2s2p\{3, 4, 5\}l$ ,  $2p^2\{3, 4, 5\}l$  ( $l < f$ ), and  $2s^2\{6, 7, 8\}s$  configurations (Aggarwal et al. 2005).

<sup>3</sup> <http://physics.nist.gov/PhysRefData/ASD/index.html>

Table 2. Level energies (Ryd) of Ne<sup>5+</sup> from different calculations, along with the compilation of NIST v4.

ID	Level	AS	NIST	MCHF <sup>v</sup>	ID	Level	AS	NIST	MCHF <sup>v</sup>	ID	Level	AS	NIST	MCHF <sup>v</sup>
1	2s <sup>2</sup> 2p <sup>2</sup> P <sub>1/2</sub>	0.0000	0.0000	0.0000	69	2s <sup>2</sup> 4d <sup>2</sup> D <sub>5/2</sub>	9.3126	9.2867	9.3197	137	2p <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	10.3493	10.3493	10.3924
2	2s <sup>2</sup> 2p <sup>2</sup> P <sub>3/2</sub>	0.0118	0.0119	0.0118	70	2p <sup>2</sup> 3s <sup>4</sup> P <sub>1/2</sub>	9.3278	9.3111	9.3432	138	2p <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	10.3504	10.3504	10.3941
3	2s <sup>2</sup> 2p <sup>2</sup> P <sub>1/2</sub>	0.8856	0.9140	0.9078	71	2p <sup>2</sup> 3s <sup>4</sup> P <sub>3/2</sub>	9.3320	9.3161	9.3473	139	2s <sup>2</sup> 2p4d <sup>4</sup> D <sub>1/2</sub>	10.3521	10.3040	10.3360
4	2s <sup>2</sup> 2p <sup>2</sup> P <sub>3/2</sub>	0.8877	0.9180	0.9119	72	2p <sup>2</sup> 3s <sup>4</sup> P <sub>5/2</sub>	9.3388	9.3247	9.3540	140	2s <sup>2</sup> 2p4d <sup>4</sup> D <sub>3/2</sub>	10.3523	10.3523	10.3362
5	2s <sup>2</sup> 2p <sup>2</sup> P <sub>5/2</sub>	0.8925	0.9239	0.9187	73	2s <sup>2</sup> 2p3d <sup>2</sup> D <sub>3/2</sub>	9.5013	9.3870	9.5176	141	2s <sup>2</sup> 2p4d <sup>4</sup> D <sub>5/2</sub>	10.3530	10.3530	10.3369
6	2s <sup>2</sup> 2p <sup>2</sup> D <sub>3/2</sub>	1.6709	1.6311	1.6799	74	2s <sup>2</sup> 2p3d <sup>2</sup> D <sub>5/2</sub>	9.5025	9.3883	9.5187	142	2s <sup>2</sup> 2p4d <sup>4</sup> D <sub>7/2</sub>	10.3563	10.3070	10.3402
7	2s <sup>2</sup> 2p <sup>2</sup> D <sub>5/2</sub>	1.6710	1.6313	1.6800	75	2p <sup>2</sup> 3s <sup>2</sup> P <sub>1/2</sub>	9.5542	9.4480	9.5461	143	2s <sup>2</sup> 2p4d <sup>4</sup> P <sub>3/2</sub>	10.3650	10.3210	10.3491
8	2s <sup>2</sup> 2p <sup>2</sup> S <sub>1/2</sub>	2.1508	2.1037	2.1959	76	2s <sup>2</sup> 2p3d <sup>2</sup> F <sub>7/2</sub>	9.5606	9.4495	9.3859	144	2s <sup>2</sup> 2p4d <sup>4</sup> P <sub>5/2</sub>	10.3677	10.3677	10.3518
9	2s <sup>2</sup> 2p <sup>2</sup> P <sub>1/2</sub>	2.3465	2.2717	2.3140	77	2s <sup>2</sup> 2p3d <sup>2</sup> F <sub>5/2</sub>	9.5607	9.4495	9.3859	145	2s <sup>2</sup> 2p4d <sup>4</sup> P <sub>1/2</sub>	10.3692	10.3230	10.3536
10	2s <sup>2</sup> 2p <sup>2</sup> P <sub>3/2</sub>	2.3545	2.2791	2.3217	78	2p <sup>2</sup> 3s <sup>2</sup> P <sub>3/2</sub>	9.5619	9.4690	9.5536	146	2s <sup>2</sup> 2p4d <sup>4</sup> D <sub>3/2</sub>	10.3705	10.3120	10.3534
11	2p <sup>3</sup> <sup>4</sup> S <sub>3/2</sub>	2.9370	2.9307	2.9706	79	2s <sup>2</sup> 2p3d <sup>2</sup> P <sub>1/2</sub>	9.5991	9.4699	9.6222	147	2s <sup>2</sup> 2p4d <sup>4</sup> D <sub>5/2</sub>	10.3728	10.3160	10.3556
12	2p <sup>3</sup> <sup>2</sup> D <sub>3/2</sub>	3.3494	3.2763	3.3347	80	2s <sup>2</sup> 2p3d <sup>2</sup> P <sub>3/2</sub>	9.6002	9.4699	9.6232	148	2p <sup>2</sup> 3d <sup>2</sup> G <sub>7/2</sub>	10.3825	10.4251	10.4251
13	2p <sup>3</sup> <sup>2</sup> P <sub>5/2</sub>	3.3497	3.2770	3.3350	81	2p <sup>2</sup> 3p <sup>2</sup> S <sub>1/2</sub>	9.6179	9.6179	9.6137	149	2p <sup>2</sup> 3d <sup>2</sup> G <sub>9/2</sub>	10.3846	10.4259	10.4259
14	2p <sup>3</sup> <sup>2</sup> P <sub>1/2</sub>	3.7997	3.6998	3.8054	82	2p <sup>2</sup> 3p <sup>4</sup> D <sub>1/2</sub>	9.6954	9.6648	9.6905	150	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	10.3882	10.3204	10.3204
15	2p <sup>3</sup> <sup>2</sup> P <sub>3/2</sub>	3.8005	3.7002	3.8063	83	2p <sup>2</sup> 3p <sup>4</sup> D <sub>3/2</sub>	9.6980	9.6675	9.6930	151	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	10.3929	10.3245	10.3245
16	2s <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	6.5626	6.5847	6.5970	84	2p <sup>2</sup> 3p <sup>4</sup> D <sub>5/2</sub>	9.7022	9.6717	9.6972	152	2p <sup>2</sup> 3d <sup>2</sup> F <sub>5/2</sub>	10.3959	10.5083	10.5083
17	2s <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	7.0079	7.0278	7.0448	85	2p <sup>2</sup> 3s <sup>2</sup> D <sub>3/2</sub>	9.7035	9.6257	9.7313	153	2p <sup>2</sup> 3d <sup>2</sup> F <sub>7/2</sub>	10.3965	10.5043	10.5043
18	2s <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	7.0110	7.0307	7.0473	86	2p <sup>2</sup> 3s <sup>2</sup> D <sub>5/2</sub>	9.7038	9.6257	9.7317	154	2p <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	10.4228	10.4056	10.4056
19	2s <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	7.4272	7.4379	7.4807	87	2p <sup>2</sup> 3p <sup>4</sup> D <sub>7/2</sub>	9.7082	9.6775	9.7032	155	2s <sup>2</sup> 2p4f <sup>4</sup> G <sub>5/2</sub>	10.4354		
20	2s <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	7.4280	7.4386	7.4815	88	2p <sup>2</sup> 3p <sup>4</sup> P <sub>1/2</sub>	9.7430	9.7103	9.7367	156	2s <sup>2</sup> 2p4f <sup>4</sup> G <sub>7/2</sub>	10.4373		
21	2s <sup>2</sup> 2p3s <sup>4</sup> P <sub>1/2</sub>	7.5851	7.5965	7.6106	89	2p <sup>2</sup> 3p <sup>4</sup> P <sub>3/2</sub>	9.7454	9.7114	9.7391	157	2s <sup>2</sup> 2p4f <sup>4</sup> G <sub>9/2</sub>	10.4403		
22	2s <sup>2</sup> 2p3s <sup>4</sup> P <sub>3/2</sub>	7.5892	7.6005	7.6146	90	2p <sup>2</sup> 3p <sup>4</sup> P <sub>5/2</sub>	9.7496	9.7184	9.7433	158	2s <sup>2</sup> 2p4d <sup>2</sup> F <sub>5/2</sub>	10.4446	10.3720	10.4208
23	2s <sup>2</sup> 2p3s <sup>4</sup> P <sub>5/2</sub>	7.5962	7.6079	7.6214	91	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	9.8218	9.7625	9.8091	159	2s <sup>2</sup> 2p4f <sup>4</sup> G <sub>11/2</sub>	10.4447		
24	2s <sup>2</sup> 2p3s <sup>2</sup> P <sub>1/2</sub>	7.8114	7.7979	7.8420	92	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	9.8291	9.7712	9.8167	160	2s <sup>2</sup> 2p4d <sup>2</sup> F <sub>7/2</sub>	10.4508	10.3790	10.4271
25	2s <sup>2</sup> 2p3s <sup>2</sup> P <sub>3/2</sub>	7.8192	7.8051	7.8495	93	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	9.9038	9.8874	9.8874	161	2s <sup>2</sup> 2p4f <sup>4</sup> F <sub>3/2</sub>	10.4553		
26	2s <sup>2</sup> 2p3p <sup>2</sup> P <sub>1/2</sub>	7.9713	7.9850	7.9990	94	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	9.9045	9.8888	9.8888	162	2s <sup>2</sup> 2p4f <sup>4</sup> F <sub>5/2</sub>	10.4561		
27	2s <sup>2</sup> 2p3p <sup>2</sup> P <sub>3/2</sub>	7.9748	7.9890	8.0025	95	2p <sup>2</sup> 3p <sup>4</sup> S <sub>3/2</sub>	9.9734	9.8699	9.9086	163	2s <sup>2</sup> 2p4f <sup>4</sup> F <sub>7/2</sub>	10.4573		
28	2s <sup>2</sup> 2p3p <sup>4</sup> D <sub>1/2</sub>	7.9919	7.9980	8.0179	96	2p <sup>2</sup> 3d <sup>4</sup> F <sub>3/2</sub>	10.0029	9.8699	10.0200	164	2s <sup>2</sup> 2p4d <sup>2</sup> P <sub>3/2</sub>	10.4588	10.4352	10.4352
29	2s <sup>2</sup> 2p3p <sup>4</sup> D <sub>3/2</sub>	7.9941	7.9998	8.0201	97	2p <sup>2</sup> 3d <sup>4</sup> F <sub>5/2</sub>	10.0050	10.0029	10.0224	165	2s <sup>2</sup> 2p4f <sup>2</sup> G <sub>9/2</sub>	10.4592	10.4391	10.4391
30	2s <sup>2</sup> 2p3p <sup>4</sup> D <sub>5/2</sub>	7.9981	8.0058	8.0240	98	2p <sup>2</sup> 3d <sup>4</sup> F <sub>7/2</sub>	10.0082	10.0082	10.0258	166	2s <sup>2</sup> 2p4d <sup>2</sup> P <sub>1/2</sub>	10.4628		
31	2s <sup>2</sup> 2p3p <sup>4</sup> D <sub>7/2</sub>	8.0041	8.0122	8.0300	99	2p <sup>2</sup> 3d <sup>4</sup> F <sub>9/2</sub>	10.0123	10.0123	10.0303	167	2s <sup>2</sup> 2p4f <sup>2</sup> G <sub>7/2</sub>	10.4681		
32	2s <sup>2</sup> 2p3p <sup>4</sup> S <sub>3/2</sub>	8.0788	8.0788	8.1061	100	2s <sup>2</sup> 2p4s <sup>4</sup> P <sub>1/2</sub>	10.0376	10.0376	10.0189	168	2s <sup>2</sup> 2p4f <sup>2</sup> G <sub>9/2</sub>	10.4726		
33	2s <sup>2</sup> 2p3p <sup>4</sup> P <sub>1/2</sub>	8.1306	8.1474	8.1800	101	2s <sup>2</sup> 2p4s <sup>4</sup> P <sub>3/2</sub>	10.0414	10.0414	10.0229	169	2s <sup>2</sup> 2p4f <sup>2</sup> G <sub>7/2</sub>	10.4819		
34	2s <sup>2</sup> 2p3p <sup>4</sup> P <sub>3/2</sub>	8.1336	8.1504	8.1827	102	2s <sup>2</sup> 2p4s <sup>4</sup> P <sub>5/2</sub>	10.0479	10.0479	10.0296	170	2s <sup>2</sup> 2p4f <sup>4</sup> D <sub>3/2</sub>	10.4844		
35	2s <sup>2</sup> 2p3p <sup>4</sup> P <sub>5/2</sub>	8.1378	8.1543	8.1866	103	2p <sup>2</sup> 3d <sup>4</sup> D <sub>1/2</sub>	10.0726	10.0726	10.0744	171	2s <sup>2</sup> 2p4f <sup>4</sup> D <sub>5/2</sub>	10.4860		
36	2s <sup>2</sup> 2p3p <sup>4</sup> D <sub>3/2</sub>	8.2059	8.2023	8.2418	104	2p <sup>2</sup> 3d <sup>4</sup> D <sub>3/2</sub>	10.0735	10.0735	10.0758	172	2s <sup>2</sup> 2p4f <sup>4</sup> D <sub>7/2</sub>	10.4869		
37	2s <sup>2</sup> 2p3p <sup>4</sup> D <sub>5/2</sub>	8.2131	8.2110	8.2490	105	2p <sup>2</sup> 3d <sup>4</sup> D <sub>5/2</sub>	10.0751	10.0751	10.0781	173	2p <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	10.5011	10.4050	10.5033
38	2s <sup>2</sup> 2p3p <sup>4</sup> S <sub>1/2</sub>	8.3490	8.3368	8.3828	106	2p <sup>2</sup> 3d <sup>4</sup> D <sub>7/2</sub>	10.0770	10.0770	10.0807	174	2p <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	10.5012	10.5035	10.5035
39	2s <sup>2</sup> 2p3d <sup>4</sup> F <sub>3/2</sub>	8.3692	8.3540	8.3809	107	2p <sup>2</sup> 3p <sup>2</sup> F <sub>5/2</sub>	10.0918	9.9862	10.0984	175	2s <sup>2</sup> 2p4f <sup>2</sup> D <sub>5/2</sub>	10.5790		
40	2s <sup>2</sup> 2p3d <sup>4</sup> F <sub>5/2</sub>	8.3715	8.3566	8.3834	108	2p <sup>2</sup> 3p <sup>2</sup> F <sub>7/2</sub>	10.0942	9.9890	10.0845	176	2s <sup>2</sup> 2p4f <sup>2</sup> D <sub>7/2</sub>	10.5791	10.4590	10.4590
41	2s <sup>2</sup> 2p3d <sup>4</sup> F <sub>7/2</sub>	8.3749	8.3621	8.3868	109	2p <sup>2</sup> 3d <sup>2</sup> P <sub>3/2</sub>	10.1044	10.1044	10.0845	177	2s <sup>2</sup> 2p4f <sup>2</sup> F <sub>7/2</sub>	10.5951		
42	2s <sup>2</sup> 2p3d <sup>4</sup> F <sub>9/2</sub>	8.3793	8.3669	8.3914	110	2p <sup>2</sup> 3d <sup>2</sup> P <sub>1/2</sub>	10.1100	10.1100	10.0900	178	2s <sup>2</sup> 2p4f <sup>2</sup> F <sub>5/2</sub>	10.5957	10.4570	10.4570
43	2s <sup>2</sup> 2p3d <sup>4</sup> D <sub>1/2</sub>	8.4651	8.4420	8.4739	111	2p <sup>2</sup> 3d <sup>2</sup> F <sub>5/2</sub>	10.1113	10.0530	10.1527	179	2p <sup>2</sup> 3d <sup>2</sup> P <sub>1/2</sub>	10.6165		10.6208
44	2s <sup>2</sup> 2p3d <sup>4</sup> D <sub>3/2</sub>	8.4658	8.4420	8.4746	112	2s <sup>2</sup> 2p4s <sup>2</sup> P <sub>1/2</sub>	10.1164	10.1164	10.0871	180	2p <sup>2</sup> 3d <sup>2</sup> P <sub>3/2</sub>	10.6193		10.6233
45	2s <sup>2</sup> 2p3d <sup>4</sup> D <sub>5/2</sub>	8.4671	8.4430	8.4759	113	2p <sup>2</sup> 3d <sup>2</sup> F <sub>7/2</sub>	10.1184	10.1184	10.1608	181	2p <sup>2</sup> 3d <sup>2</sup> S <sub>1/2</sub>	10.6838		10.6831
46	2s <sup>2</sup> 2p3d <sup>4</sup> D <sub>7/2</sub>	8.4694	8.4457	8.4782	114	2s <sup>2</sup> 2p4s <sup>2</sup> P <sub>3/2</sub>	10.1222	10.1222	10.0931	182	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	10.8101		10.8195
47	2s <sup>2</sup> 2p3d <sup>4</sup> D <sub>9/2</sub>	8.4892	8.4568	8.5025	115	2p <sup>2</sup> 3d <sup>4</sup> P <sub>5/2</sub>	10.1866	10.1866	10.1628	183	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	10.8112		10.8208

Notes. <sup>(a)</sup> MCHF calculation from the work of Mitrík et al. (2001).

Table 3. Level energies (Ryd) of Ar<sup>13+</sup> from different calculations, along with the compilation of NIST v4.

ID	Level	AS	NIST	Grasp <sup>a</sup>	ID	Level	AS	NIST	Grasp <sup>a</sup>	ID	Level	AS	NIST	Grasp <sup>a</sup>
1	2s <sup>2</sup> 2p <sup>2</sup> 2P <sub>1/2</sub>	0	0.0000	0.0000	69	2p <sup>2</sup> 3s <sup>2</sup> P <sub>1/2</sub>	37.5209	37.5209	37.5292	137	2s2p4s <sup>2</sup> P <sub>3/2</sub>	44.7689	44.7689	44.6686
2	2s <sup>2</sup> 2p <sup>2</sup> 2P <sub>3/2</sub>	0.2042	0.2065	0.2055	70	2s2p3d <sup>2</sup> D <sub>5/2</sub>	37.5231	37.5231	37.4763	138	2s2p4p <sup>4</sup> D <sub>1/2</sub>	44.8047	44.8047	44.6978
3	2s2p <sup>2</sup> 4P <sub>1/2</sub>	2.0487	2.0986	2.0602	71	2p <sup>2</sup> 3s <sup>2</sup> P <sub>3/2</sub>	37.6311	37.6311	37.6372	139	2s2p4p <sup>4</sup> D <sub>3/2</sub>	44.8466	44.8466	44.7408
4	2s2p <sup>2</sup> 4P <sub>3/2</sub>	2.1269	2.1775	2.1379	72	2s2p3d <sup>2</sup> P <sub>1/2</sub>	37.6810	37.6810	37.6364	140	2s2p4p <sup>2</sup> P <sub>3/2</sub>	44.9044	44.9044	44.7968
5	2s2p <sup>2</sup> 4P <sub>5/2</sub>	2.2390	2.2820	2.2422	73	2s2p3d <sup>2</sup> P <sub>3/2</sub>	37.7054	37.7054	37.6586	141	2s2p4p <sup>4</sup> D <sub>5/2</sub>	44.9078	44.9078	44.8038
6	2s2p <sup>2</sup> 2D <sub>3/2</sub>	3.7691	3.7385	3.7798	74	2p <sup>2</sup> 3p <sup>2</sup> S <sub>1/2</sub>	37.7337	37.7337	37.6969	142	2s2p4p <sup>2</sup> P <sub>1/2</sub>	44.9231	44.9231	44.8158
7	2s2p <sup>2</sup> 2D <sub>5/2</sub>	3.7809	3.7471	3.7879	75	2p <sup>2</sup> 3p <sup>4</sup> D <sub>1/2</sub>	37.8113	37.8113	37.7775	143	2s2p4p <sup>4</sup> P <sub>1/2</sub>	44.9728	44.9728	44.8683
8	2s2p <sup>2</sup> 2S <sub>1/2</sub>	4.7322	4.6876	4.7584	76	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	37.8531	37.8531	37.8183	144	2s2p4p <sup>4</sup> S <sub>3/2</sub>	44.9989	44.9989	44.8939
9	2s2p <sup>2</sup> 2P <sub>1/2</sub>	5.0260	4.9686	5.0489	77	2p <sup>2</sup> 3s <sup>2</sup> D <sub>5/2</sub>	37.8903	37.8903	37.9098	145	2s2p4p <sup>4</sup> D <sub>7/2</sub>	45.0193	45.0193	44.9248
10	2s2p <sup>2</sup> 2P <sub>3/2</sub>	5.1212	5.0546	5.1382	78	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	37.9052	37.9052	37.9252	146	2s2p4p <sup>4</sup> P <sub>3/2</sub>	45.0777	45.0777	44.9822
11	2p <sup>3</sup> 4S <sub>3/2</sub>	6.5409	6.5513	6.5551	79	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	37.9303	37.9303	37.8961	147	2s2p4p <sup>4</sup> P <sub>5/2</sub>	45.0901	45.0901	44.9931
12	2p <sup>3</sup> 2D <sub>3/2</sub>	7.4504	7.3848	7.4625	80	2p <sup>2</sup> 3p <sup>4</sup> P <sub>1/2</sub>	38.0183	38.0183	37.9839	148	2s2p4p <sup>2</sup> D <sub>3/2</sub>	45.1040	45.1040	45.0026
13	2p <sup>3</sup> 2D <sub>5/2</sub>	7.4754	7.4082	7.4785	81	2p <sup>2</sup> 3p <sup>4</sup> P <sub>3/2</sub>	38.0275	38.0275	37.9903	149	2s2p4d <sup>4</sup> F <sub>3/2</sub>	45.1507	45.1507	45.0389
14	2p <sup>3</sup> 2P <sub>1/2</sub>	8.3694	8.2815	8.3882	82	2p <sup>2</sup> 3p <sup>2</sup> D <sub>7/2</sub>	38.0846	38.0846	38.0481	150	2s2p4d <sup>4</sup> F <sub>5/2</sub>	45.1812	45.1812	45.0696
15	2p <sup>3</sup> 2P <sub>3/2</sub>	8.4117	8.3204	8.4259	83	2p <sup>2</sup> 3p <sup>4</sup> P <sub>5/2</sub>	38.1537	38.1537	38.1159	151	2s2p4p <sup>2</sup> D <sub>5/2</sub>	45.1930	45.1930	45.0939
16	2s <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	31.1413	31.1413	31.0761	84	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	38.1537	38.1537	38.1159	152	2s2p4d <sup>4</sup> F <sub>7/2</sub>	45.2332	45.2332	45.1230
17	2s <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	32.1745	32.2032	32.1137	85	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	38.2960	38.2960	38.2631	153	2s2p4d <sup>4</sup> P <sub>5/2</sub>	45.2639	45.2639	45.1525
18	2s <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	32.2315	32.2118	32.1704	86	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	38.4492	38.4492	38.4071	154	2s2p4d <sup>4</sup> D <sub>3/2</sub>	45.2810	45.2810	45.1708
19	2s <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	33.2077	33.174	33.1377	87	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	38.4796	38.4796	38.4437	155	2s2p4d <sup>4</sup> D <sub>1/2</sub>	45.2887	45.2887	45.1793
20	2s <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	33.2250	33.186	33.1534	88	2p <sup>2</sup> 3p <sup>4</sup> S <sub>3/2</sub>	38.4996	38.4996	38.4344	156	2s2p4p <sup>2</sup> S <sub>1/2</sub>	45.2917	45.2917	45.1874
21	2s2p3s <sup>4</sup> P <sub>1/2</sub>	33.2554	33.2260	33.2260	89	2p <sup>2</sup> 3d <sup>4</sup> F <sub>3/2</sub>	38.6220	38.6220	38.5675	157	2s2p4d <sup>4</sup> F <sub>9/2</sub>	45.3367	45.3367	45.2354
22	2s2p3s <sup>4</sup> P <sub>3/2</sub>	33.3203	33.2854	33.2905	90	2p <sup>2</sup> 3d <sup>4</sup> F <sub>5/2</sub>	38.7231	38.7231	38.6681	158	2s2p4d <sup>2</sup> D <sub>3/2</sub>	45.3381	45.3381	45.2673
23	2s2p3s <sup>4</sup> P <sub>5/2</sub>	33.4459	33.4059	33.4203	91	2p <sup>2</sup> 3d <sup>4</sup> F <sub>7/2</sub>	38.7749	38.7749	38.6808	159	2s2p4d <sup>2</sup> D <sub>5/2</sub>	45.3749	45.3749	45.2936
24	2s2p3s <sup>2</sup> P <sub>1/2</sub>	33.7854	33.770	33.7704	92	2p <sup>2</sup> 3p <sup>2</sup> F <sub>5/2</sub>	38.8036	38.8036	38.7472	160	2s2p4d <sup>4</sup> D <sub>7/2</sub>	45.3949	45.3949	45.2936
25	2s2p3s <sup>2</sup> P <sub>3/2</sub>	33.9241	33.907	33.9114	93	2p <sup>2</sup> 3d <sup>4</sup> F <sub>9/2</sub>	38.8171	38.8171	38.7860	161	2s2p4f <sup>4</sup> G <sub>5/2</sub>	45.4064	45.4064	45.2902
26	2s2p3p <sup>4</sup> D <sub>1/2</sub>	34.1806	34.1806	34.1368	94	2p <sup>2</sup> 3p <sup>2</sup> F <sub>7/2</sub>	38.8390	38.8390	38.7872	162	2s2p4f <sup>4</sup> F <sub>7/2</sub>	45.4115	45.4115	45.2953
27	2s2p3p <sup>4</sup> D <sub>3/2</sub>	34.2389	34.2389	34.1935	95	2p <sup>2</sup> 3d <sup>4</sup> P <sub>3/2</sub>	38.8496	38.8496	38.8025	163	2s2p4d <sup>4</sup> D <sub>5/2</sub>	45.4308	45.4308	45.3315
28	2s2p3p <sup>2</sup> P <sub>1/2</sub>	34.3050	34.3050	34.2670	96	2p <sup>2</sup> 3d <sup>4</sup> D <sub>1/2</sub>	38.8824	38.8824	38.8298	164	2s2p4d <sup>2</sup> P <sub>3/2</sub>	45.4367	45.4367	45.3386
29	2s2p3p <sup>2</sup> P <sub>3/2</sub>	34.3263	34.3263	34.2885	97	2p <sup>2</sup> 3d <sup>4</sup> D <sub>3/2</sub>	38.9205	38.9205	38.8681	165	2s2p4d <sup>4</sup> P <sub>1/2</sub>	45.4713	45.4713	45.3560
30	2s2p3p <sup>4</sup> D <sub>5/2</sub>	34.3357	34.3357	34.2915	98	2p <sup>2</sup> 3d <sup>4</sup> D <sub>5/2</sub>	38.9276	38.9276	38.8788	166	2s2p4f <sup>4</sup> F <sub>3/2</sub>	45.4553	45.4553	45.3422
31	2s2p3p <sup>4</sup> D <sub>7/2</sub>	34.4471	34.4471	34.4066	99	2p <sup>2</sup> 3d <sup>4</sup> D <sub>7/2</sub>	38.9276	38.9276	38.8788	167	2s2p4f <sup>4</sup> F <sub>5/2</sub>	45.4629	45.4629	45.3485
32	2s2p3p <sup>4</sup> S <sub>3/2</sub>	34.5295	34.5295	34.4901	100	2p <sup>2</sup> 3d <sup>2</sup> F <sub>5/2</sub>	38.9692	38.9692	38.9235	168	2s2p4f <sup>4</sup> F <sub>7/2</sub>	45.4654	45.4654	45.3509
33	2s2p3p <sup>2</sup> P <sub>1/2</sub>	34.5983	34.5983	34.6001	101	2p <sup>2</sup> 3d <sup>2</sup> F <sub>7/2</sub>	39.0329	39.0329	38.9860	169	2s2p4f <sup>2</sup> F <sub>7/2</sub>	45.4713	45.4713	45.3560
34	2s2p3p <sup>4</sup> P <sub>3/2</sub>	34.6747	34.6747	34.6734	102	2p <sup>2</sup> 3d <sup>2</sup> F <sub>9/2</sub>	39.1120	39.1120	39.0710	170	2s2p4f <sup>2</sup> F <sub>5/2</sub>	45.4995	45.4995	45.3846
35	2s2p3p <sup>4</sup> P <sub>5/2</sub>	34.7237	34.7237	34.7226	103	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	39.1312	39.1312	39.0691	171	2s2p4f <sup>2</sup> G <sub>7/2</sub>	45.5006	45.5006	45.3863
36	2s2p3p <sup>2</sup> D <sub>3/2</sub>	34.7765	34.7765	34.7586	104	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	39.1428	39.1428	39.0760	172	2s2p4d <sup>2</sup> F <sub>5/2</sub>	45.5250	45.5250	45.4170
37	2s2p3p <sup>2</sup> D <sub>5/2</sub>	34.9012	34.9012	34.8907	105	2p <sup>2</sup> 3d <sup>4</sup> P <sub>5/2</sub>	39.1655	39.1655	39.1089	173	2s2p4d <sup>2</sup> P <sub>3/2</sub>	45.5864	45.5864	45.4808
38	2s2p3d <sup>4</sup> F <sub>3/2</sub>	35.0879	35.0879	35.0216	106	2p <sup>2</sup> 3d <sup>4</sup> P <sub>3/2</sub>	39.2075	39.2075	39.1535	174	2s2p4f <sup>4</sup> G <sub>9/2</sub>	45.5976	45.5976	45.4937
39	2s2p3d <sup>4</sup> F <sub>5/2</sub>	35.1274	35.1274	35.0603	107	2p <sup>2</sup> 3d <sup>2</sup> P <sub>1/2</sub>	39.2208	39.2208	39.1733	175	2s2p4d <sup>2</sup> F <sub>7/2</sub>	45.6032	45.6032	45.4994
40	2s2p3p <sup>2</sup> S <sub>1/2</sub>	35.1719	35.1719	35.1594	108	2p <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	39.2456	39.2456	39.2393	176	2s2p4d <sup>2</sup> F <sub>7/2</sub>	45.6140	45.6140	45.5083
41	2s2p3d <sup>4</sup> F <sub>7/2</sub>	35.1869	35.1869	35.1203	109	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	39.3396	39.3396	39.2804	177	2s2p4f <sup>4</sup> G <sub>11/2</sub>	45.6166	45.6166	45.5121
42	2s2p3d <sup>4</sup> F <sub>9/2</sub>	35.2756	35.2756	35.2137	110	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	39.4393	39.4393	39.3833	178	2s2p4f <sup>4</sup> D <sub>5/2</sub>	45.6192	45.6192	45.5151
43	2s2p3d <sup>4</sup> D <sub>5/2</sub>	35.3938	35.3938	35.3228	111	2p <sup>2</sup> 3d <sup>2</sup> G <sub>7/2</sub>	39.5719	39.5719	39.5341	179	2s2p4f <sup>4</sup> D <sub>7/2</sub>	45.6223	45.6223	45.5180
44	2s2p3d <sup>4</sup> D <sub>3/2</sub>	35.4004	35.4004	35.3304	112	2p <sup>2</sup> 3d <sup>2</sup> G <sub>9/2</sub>	39.5943	39.5943	39.5529	180	2s2p4f <sup>4</sup> D <sub>3/2</sub>	45.6383	45.6383	45.5346
45	2s2p3d <sup>4</sup> D <sub>1/2</sub>	35.4017	35.4017	35.3326	113	2p <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	39.6243	39.6243	39.5672	181	2s2p4d <sup>2</sup> P <sub>1/2</sub>	45.6392	45.6392	45.5358
46	2s2p3s <sup>2</sup> P <sub>1/2</sub>	35.4221	35.4221	35.4359	114	2p <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	39.6340	39.6340	39.5765	182	2s2p4f <sup>2</sup> G <sub>9/2</sub>	45.6448	45.6448	45.5417
47	2s2p3s <sup>2</sup> P <sub>3/2</sub>	35.4253	35.4253	35.4455	115	2p <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	39.8090	39.8090	39.7694	183	2s2p4f <sup>4</sup> D <sub>1/2</sub>	45.6497	45.6497	45.5466

Notes. <sup>(a)</sup> GRASP calculation from the work of Aggarwal et al. (2005).

Table 4. Level energies (Ryd) of Fe<sup>21+</sup> from different calculations, along with the compilation of NIST v4.

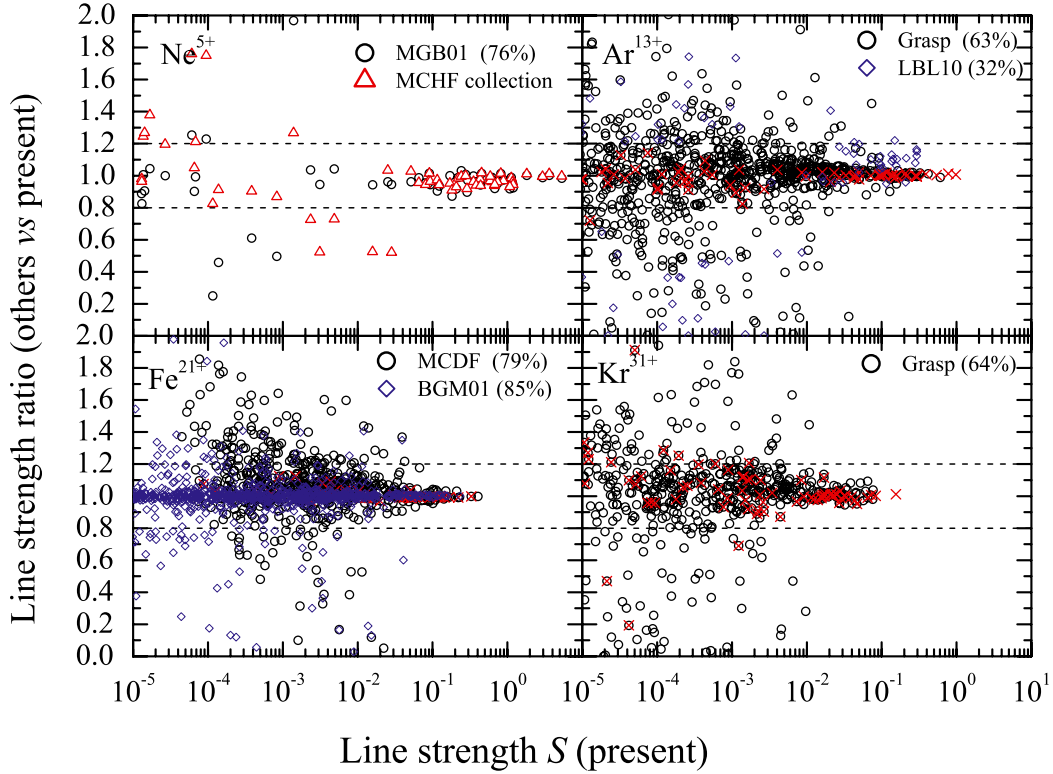
ID	Level	AS	NIST	MCDF <sup>a</sup>	ID	Level	AS	NIST	MCDF <sup>a</sup>	ID	Level	AS	NIST	MCDF <sup>a</sup>
1	2s <sup>2</sup> 2p <sup>2</sup> P <sub>1/2</sub>	0	0	0.0000	69	2p <sup>2</sup> 3p <sup>4</sup> D <sub>1/2</sub>	84.5624	84.5624	84.4349	137	2s2p4p <sup>4</sup> D <sub>3/2</sub>	104.4113		104.1392
2	2s <sup>2</sup> 2p <sup>2</sup> P <sub>3/2</sub>	1.0603	1.0777	1.0749	70	2s2p3d <sup>2</sup> D <sub>3/2</sub>	84.5817	84.5817	84.4171	138	2s2p4p <sup>4</sup> S <sub>3/2</sub>	104.5214		104.2467
3	2s2p <sup>2</sup> 4P <sub>1/2</sub>	3.6179	3.6865	3.6715	71	2s2p3d <sup>2</sup> D <sub>5/2</sub>	84.7042	84.7042	84.5368	139	2s2p4s <sup>4</sup> P <sub>5/2</sub>	104.6367		104.4038
4	2s2p <sup>2</sup> 4P <sub>3/2</sub>	4.1160	4.1936	4.1739	72	2p <sup>2</sup> 3s <sup>2</sup> P <sub>3/2</sub>	84.7790	84.7790	84.7350	140	2s2p4p <sup>4</sup> P <sub>1/2</sub>	104.6684		104.4069
5	2s2p <sup>2</sup> 4F <sub>5/2</sub>	4.6268	4.6772	4.6592	73	2s2p3d <sup>2</sup> P <sub>1/2</sub>	84.8978	84.8978	84.7374	141	2s2p4p <sup>4</sup> D <sub>5/2</sub>	104.6745		104.4069
6	2s2p <sup>2</sup> 2D <sub>3/2</sub>	6.7138	6.7097	6.7573	74	2s2p3d <sup>2</sup> P <sub>3/2</sub>	84.9134	84.9134	84.7548	142	2s2p4p <sup>2</sup> P <sub>1/2</sub>	104.7030	104.4770	104.4356
7	2s2p <sup>2</sup> 2D <sub>5/2</sub>	6.9224	6.9184	6.9597	75	2p <sup>2</sup> 3p <sup>4</sup> D <sub>3/2</sub>	85.0519	85.0519	84.9179	143	2s2p4p <sup>2</sup> D <sub>3/2</sub>	104.7944	104.5590	104.5288
8	2s2p <sup>2</sup> 2P <sub>1/2</sub>	7.7937	7.7790	7.8543	76	2p <sup>2</sup> 3p <sup>2</sup> S <sub>1/2</sub>	85.0774	85.0774	84.9893	144	2s2p4s <sup>2</sup> P <sub>3/2</sub>	104.8556		104.6279
9	2s2p <sup>2</sup> 2S <sub>1/2</sub>	8.9126	8.9154	8.9875	77	2p <sup>2</sup> 3p <sup>4</sup> P <sub>3/2</sub>	85.4102	85.4102	85.2964	145	2s2p4d <sup>4</sup> F <sub>3/2</sub>	104.8838		104.5975
10	2s2p <sup>2</sup> 2P <sub>3/2</sub>	9.0649	9.0427	9.1189	78	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	85.4840	85.4840	85.3815	146	2s2p4d <sup>4</sup> F <sub>5/2</sub>	104.9892	104.7230	104.7029
11	2p <sup>3</sup> 4S <sub>3/2</sub>	11.3938	11.4428	11.4835	79	2p <sup>2</sup> 3s <sup>2</sup> D <sub>3/2</sub>	85.5691	85.5691	85.5353	147	2s2p4d <sup>4</sup> P <sub>5/2</sub>	105.1786		104.8957
12	2p <sup>3</sup> 2D <sub>3/2</sub>	12.7219	12.7223	12.8095	80	2p <sup>2</sup> 3p <sup>4</sup> P <sub>1/2</sub>	85.6311	85.6311	85.5281	148	2s2p4d <sup>4</sup> F <sub>7/2</sub>	105.2299		104.9450
13	2p <sup>3</sup> 2D <sub>5/2</sub>	13.0256	12.9999	13.0827	81	2p <sup>2</sup> 3p <sup>4</sup> P <sub>3/2</sub>	85.6854	85.6854	85.5701	149	2s2p4d <sup>4</sup> D <sub>3/2</sub>	105.2456	105.0330	104.9663
14	2p <sup>3</sup> 2P <sub>1/2</sub>	14.3269	14.3035	14.4203	82	2p <sup>2</sup> 3s <sup>2</sup> D <sub>5/2</sub>	85.7357	85.7357	85.7201	150	2s2p4d <sup>4</sup> D <sub>1/2</sub>	105.2721		104.9952
15	2p <sup>3</sup> 2P <sub>3/2</sub>	14.8546	14.8329	14.9376	83	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	85.8232	85.8232	85.7121	151	2s2p4f <sup>4</sup> G <sub>5/2</sub>	105.2994		104.9986
16	2s <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	74.0596		73.9173	84	2p <sup>2</sup> 3p <sup>4</sup> D <sub>7/2</sub>	85.9122	85.9122	85.7926	152	2s2p4f <sup>4</sup> D <sub>7/2</sub>	105.3225		105.0197
17	2s <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	75.7060		75.5693	85	2p <sup>2</sup> 3d <sup>4</sup> F <sub>3/2</sub>	86.2029	86.2029	86.0427	153	2s2p4p <sup>4</sup> P <sub>3/2</sub>	105.3669		105.1482
18	2s <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	76.0015		75.8716	86	2p <sup>2</sup> 3p <sup>4</sup> S <sub>3/2</sub>	86.3421	86.3421	86.2111	154	2s2p4p <sup>4</sup> D <sub>7/2</sub>	105.3806		105.1590
19	2s2p3s <sup>4</sup> P <sub>1/2</sub>	77.3238		77.2006	87	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	86.4269	86.4269	86.3172	155	2s2p4d <sup>2</sup> D <sub>3/2</sub>	105.3863		105.1110
20	2s <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	77.5321	77.4390	77.3765	88	2p <sup>2</sup> 3d <sup>4</sup> F <sub>5/2</sub>	86.4297	86.4297	86.2656	156	2s2p4p <sup>4</sup> P <sub>5/2</sub>	105.4009		105.1821
21	2s2p3s <sup>4</sup> P <sub>3/2</sub>	77.6028		77.4663	89	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	86.4014	86.4014	86.3180	157	2s2p4d <sup>2</sup> F <sub>5/2</sub>	105.4523	105.3240	105.1722
22	2s <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	77.6273	77.5210	77.4663	90	2p <sup>2</sup> 3d <sup>4</sup> F <sub>7/2</sub>	86.7021	86.7021	86.6090	158	2s2p4p <sup>2</sup> P <sub>3/2</sub>	105.4671		105.2461
23	2s2p3s <sup>2</sup> P <sub>1/2</sub>	78.2248		78.1605	91	2p <sup>2</sup> 3d <sup>4</sup> F <sub>5/2</sub>	86.8421	86.8421	86.7002	159	2s2p4f <sup>4</sup> F <sub>3/2</sub>	105.5584		105.2649
24	2s2p3s <sup>4</sup> P <sub>3/2</sub>	78.3315		78.2274	92	2p <sup>2</sup> 3d <sup>2</sup> P <sub>3/2</sub>	86.8509	86.8509	86.7206	160	2s2p4f <sup>4</sup> G <sub>7/2</sub>	105.5734		105.2744
25	2s2p3p <sup>4</sup> D <sub>1/2</sub>	78.7826		78.6446	93	2p <sup>2</sup> 3d <sup>4</sup> D <sub>1/2</sub>	86.9166	86.9166	86.8019	161	2s2p4f <sup>4</sup> D <sub>3/2</sub>	105.5769		105.2809
26	2s2p3s <sup>2</sup> P <sub>3/2</sub>	79.0038		78.9506	94	2p <sup>2</sup> 3d <sup>4</sup> D <sub>5/2</sub>	86.9225	86.9225	86.7780	162	2s2p4f <sup>4</sup> G <sub>9/2</sub>	105.5812		105.2812
27	2s2p3p <sup>4</sup> D <sub>3/2</sub>	79.0315		78.8880	95	2p <sup>2</sup> 3p <sup>2</sup> F <sub>5/2</sub>	87.1006	87.1006	87.0175	163	2s2p4p <sup>2</sup> D <sub>3/2</sub>	105.6051		105.4045
28	2s2p3p <sup>2</sup> P <sub>3/2</sub>	79.3539		79.2392	96	2p <sup>2</sup> 3d <sup>4</sup> D <sub>7/2</sub>	87.1807	87.1807	87.0348	164	2s2p4f <sup>2</sup> F <sub>5/2</sub>	105.6399		105.3291
29	2s2p3p <sup>2</sup> P <sub>1/2</sub>	79.4356		79.3193	97	2p <sup>2</sup> 3d <sup>4</sup> F <sub>9/2</sub>	87.2052	87.2052	87.0496	165	2s2p4f <sup>2</sup> G <sub>7/2</sub>	105.6411		105.3407
30	2s2p3p <sup>4</sup> D <sub>5/2</sub>	79.4736		79.3473	98	2p <sup>2</sup> 3d <sup>4</sup> D <sub>3/2</sub>	87.2133	87.2133	87.0765	166	2s2p4p <sup>2</sup> S <sub>1/2</sub>	105.7184		105.5042
31	2s2p3p <sup>4</sup> P <sub>1/2</sub>	79.6472		79.5906	99	2p <sup>2</sup> 3d <sup>2</sup> F <sub>5/2</sub>	87.2391	87.2391	87.0956	167	2s2p4d <sup>4</sup> F <sub>9/2</sub>	105.9131		105.6748
32	2s2p3p <sup>2</sup> D <sub>3/2</sub>	79.8289		79.7219	100	2p <sup>2</sup> 3p <sup>2</sup> F <sub>7/2</sub>	87.2453	87.2453	87.1529	168	2s2p4d <sup>4</sup> D <sub>7/2</sub>	105.9815	105.8710	105.7483
33	2s2p3p <sup>4</sup> D <sub>7/2</sub>	80.1306		80.0262	101	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	87.4384	87.4384	87.3288	169	2s2p4d <sup>4</sup> D <sub>5/2</sub>	106.0086	105.8710	105.7785
34	2s2p3p <sup>4</sup> P <sub>3/2</sub>	80.1878		80.1167	102	2p <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	87.5428	87.5428	87.5069	170	2s2p4d <sup>4</sup> P <sub>3/2</sub>	106.0348		105.8077
35	2s2p3p <sup>4</sup> S <sub>3/2</sub>	80.3448		80.2814	103	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	87.5843	87.5843	87.4601	171	2s2p4d <sup>4</sup> P <sub>1/2</sub>	106.0445		105.8212
36	2s2p3p <sup>4</sup> S <sub>5/2</sub>	80.3676		80.2813	104	2p <sup>2</sup> 3d <sup>4</sup> P <sub>3/2</sub>	87.6294	87.6294	87.4803	172	2s2p4d <sup>2</sup> D <sub>3/2</sub>	106.1261	105.8070	105.8957
37	2s2p3d <sup>4</sup> F <sub>3/2</sub>	80.4412		80.2645	105	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	87.7101	87.7101	87.5900	173	2s2p4d <sup>2</sup> P <sub>3/2</sub>	106.2272		105.9998
38	2s2p3d <sup>4</sup> F <sub>5/2</sub>	80.6206		80.4371	106	2p <sup>2</sup> 3d <sup>4</sup> P <sub>3/2</sub>	87.7533	87.7533	87.6056	174	2s2p4d <sup>2</sup> F <sub>7/2</sub>	106.3120	106.1530	106.0809
39	2s2p3p <sup>2</sup> D <sub>5/2</sub>	80.7846	80.6020	80.7160	107	2p <sup>2</sup> 3d <sup>2</sup> P <sub>1/2</sub>	87.7737	87.7737	87.6772	175	2s2p4f <sup>4</sup> F <sub>7/2</sub>	106.3383		106.0936
40	2s2p3d <sup>4</sup> P <sub>1/2</sub>	80.9030	80.7750	80.7167	108	2p <sup>2</sup> 3d <sup>4</sup> P <sub>1/2</sub>	87.8428	87.8428	87.7002	176	2s2p4f <sup>4</sup> F <sub>9/2</sub>	106.3419		106.0959
41	2s2p3d <sup>4</sup> F <sub>7/2</sub>	81.0112	80.8660	80.8151	109	2p <sup>2</sup> 3d <sup>2</sup> F <sub>7/2</sub>	87.8895	87.8895	87.7481	177	2s2p4f <sup>4</sup> F <sub>5/2</sub>	106.3576		106.1146
42	2s2p3p <sup>2</sup> S <sub>1/2</sub>	81.0709		80.9981	110	2p <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	88.2743	88.2743	88.0947	178	2s2p4d <sup>2</sup> P <sub>1/2</sub>	106.3625		106.1395
43	2s2p3d <sup>4</sup> D <sub>3/2</sub>	81.0919	80.9390	80.9045	111	2p <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	88.2917	88.2917	88.1252	179	2s2p4f <sup>2</sup> F <sub>7/2</sub>	106.3803		106.1337
44	2s2p3s <sup>2</sup> P <sub>1/2</sub>	81.0922		81.0242	112	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	88.3428	88.3428	88.2462	180	2s2p4f <sup>2</sup> G <sub>11/2</sub>	106.3822		106.1341
45	2s2p3s <sup>2</sup> P <sub>3/2</sub>	81.1217		81.0382	113	2p <sup>2</sup> 3d <sup>2</sup> G <sub>7/2</sub>	88.4228	88.4228	88.3161	181	2s2p4f <sup>4</sup> D <sub>3/2</sub>	106.3931		106.1525
46	2s2p3d <sup>4</sup> D <sub>1/2</sub>	81.1303	80.9930	80.9331	114	2p <sup>2</sup> 3d <sup>2</sup> G <sub>9/2</sub>	88.5818	88.5818	88.4689	182	2s2p4f <sup>4</sup> D <sub>1/2</sub>	106.4193		106.1807
47	2s2p3d <sup>2</sup> D <sub>3/2</sub>	81.4192		81.2526	115	2p <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	88.8144	88.8144	88.7219	183	2s2p4f <sup>2</sup> G <sub>9/2</sub>	106.4221		106.1708

Notes. <sup>(a)</sup> MCDF calculation from the work of Jonauskas et al. (2006).

Table 5. Level energies (Ryd) of Kr<sup>31+</sup> from different calculations, along with the compilation of NIST v4.

ID	Level	AS	NIST	Grasp <sup>d</sup>	ID	Level	AS	NIST	Grasp <sup>d</sup>	ID	Level	AS	NIST	Grasp <sup>d</sup>
1	2s <sup>2</sup> p <sup>2</sup> P <sub>1/2</sub>	0	4.4885	4.4815	69	2p <sup>2</sup> 3s <sup>2</sup> D <sub>3/2</sub>	173.0067	172.9762	172.9762	137	2s2p4p <sup>4</sup> D <sub>3/2</sub>	215.5095		215.5095
2	2s <sup>2</sup> p <sup>2</sup> F <sub>3/2</sub>	4.3704	6.3610	6.3565	70	2s2p3d <sup>2</sup> F <sub>5/2</sub>	173.0532	173.0532	173.0532	138	2s2p4p <sup>4</sup> S <sub>3/2</sub>	215.6725		215.6725
3	2s2p <sup>2</sup> P <sub>1/2</sub>	6.2363	9.0192	9.2119	71	2s2p3d <sup>2</sup> D <sub>3/2</sub>	173.1556	173.1556	173.1556	139	2s2p4p <sup>4</sup> P <sub>1/2</sub>	215.9596		215.9596
4	2s2p <sup>2</sup> F <sub>3/2</sub>	9.0192	10.3924	10.5128	72	2s2p3d <sup>2</sup> F <sub>7/2</sub>	173.1636	173.1636	173.1636	140	2s2p4d <sup>4</sup> F <sub>3/2</sub>	216.2201		216.2201
5	2s2p <sup>2</sup> P <sub>3/2</sub>	12.9065	13.0261	13.0933	73	2s2p3d <sup>2</sup> P <sub>1/2</sub>	173.5070	173.5070	173.5070	141	2s2p4p <sup>4</sup> D <sub>5/2</sub>	216.2695		216.2695
6	2s2p <sup>2</sup> D <sub>3/2</sub>	13.5508	15.2786	15.2515	74	2p <sup>2</sup> 3p <sup>2</sup> S <sub>1/2</sub>	173.6190	173.6190	173.6190	142	2s2p4p <sup>2</sup> P <sub>1/2</sub>	216.2879		216.2879
7	2s2p <sup>2</sup> P <sub>1/2</sub>	18.2289	18.4936	18.5671	75	2s2p3d <sup>2</sup> D <sub>5/2</sub>	173.6270	173.6270	173.6270	143	2s2p4p <sup>2</sup> D <sub>3/2</sub>	216.3746		216.3746
8	2s2p <sup>2</sup> D <sub>5/2</sub>	18.3739	18.5837	18.6795	76	2p <sup>2</sup> 3d <sup>4</sup> F <sub>3/2</sub>	173.7606	173.7606	173.7606	144	2s2p4d <sup>4</sup> P <sub>5/2</sub>	216.4855		216.4855
9	2s2p <sup>2</sup> S <sub>1/2</sub>	20.3589	20.6545	20.6545	77	2s2p3p <sup>4</sup> P <sub>3/2</sub>	174.0082	174.0082	174.0082	145	2s2p4f <sup>4</sup> G <sub>5/2</sub>	216.9139		216.9139
10	2s2p <sup>2</sup> P <sub>3/2</sub>	23.7137	24.0917	24.0917	78	2p <sup>2</sup> 3p <sup>4</sup> P <sub>3/2</sub>	174.5572	174.5572	174.5572	146	2s2p4f <sup>4</sup> F <sub>5/2</sub>	216.9587		216.9587
11	2p <sup>3</sup> 4S <sub>3/2</sub>	24.7156	24.9988	25.0107	79	2p <sup>2</sup> 3p <sup>4</sup> F <sub>5/2</sub>	174.5847	174.5847	174.5847	147	2s2p4f <sup>4</sup> D <sub>7/2</sub>	217.0004		217.0004
12	2p <sup>3</sup> 2D <sub>3/2</sub>	26.4644	29.8285	26.8755	80	2p <sup>2</sup> 3p <sup>4</sup> P <sub>5/2</sub>	175.0521	175.0521	175.0521	148	2s2p4d <sup>4</sup> D <sub>3/2</sub>	217.1050		217.1050
13	2p <sup>3</sup> 2D <sub>5/2</sub>	29.8285	30.1338	30.2731	81	2p <sup>2</sup> 3p <sup>4</sup> D <sub>5/2</sub>	175.2453	175.2453	175.2453	149	2s2p4d <sup>4</sup> D <sub>1/2</sub>	217.1475		217.1475
14	2p <sup>3</sup> 2P <sub>1/2</sub>	154.6114	157.0706	159.0764	82	2p <sup>2</sup> 3p <sup>4</sup> P <sub>1/2</sub>	175.4975	175.4975	175.4975	150	2s2p4d <sup>4</sup> F <sub>7/2</sub>	217.2121		217.2121
15	2p <sup>3</sup> 2P <sub>3/2</sub>	160.4971	160.8956	160.6793	83	2p <sup>2</sup> 3p <sup>4</sup> D <sub>3/2</sub>	175.8832	175.8832	175.8832	151	2s2p4d <sup>2</sup> D <sub>3/2</sub>	217.3858		217.3858
16	2s <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	161.5522	162.2666	161.8959	84	2p <sup>2</sup> 3s <sup>2</sup> D <sub>5/2</sub>	176.6630	176.6630	176.6630	152	2s2p4d <sup>2</sup> F <sub>5/2</sub>	217.4336		217.4336
17	2s <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	162.2666	163.2112	162.9443	85	2p <sup>2</sup> 3p <sup>4</sup> D <sub>7/2</sub>	176.7150	176.7150	176.7150	153	2s2p4f <sup>4</sup> F <sub>3/2</sub>	217.6655		217.6655
18	2s <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	163.1852	163.2112	163.0068	86	2p <sup>2</sup> 3p <sup>4</sup> P <sub>3/2</sub>	176.3562	176.3562	176.3562	154	2s2p4f <sup>4</sup> G <sub>7/2</sub>	217.6753		217.6753
19	2s2p3s <sup>4</sup> P <sub>1/2</sub>	163.2112	163.2112	163.0068	87	2p <sup>2</sup> 3s <sup>2</sup> D <sub>5/2</sub>	177.0666	177.0666	177.0666	155	2s2p4f <sup>4</sup> D <sub>5/2</sub>	217.7037		217.7037
20	2s2p3s <sup>4</sup> P <sub>3/2</sub>	163.2112	163.2112	163.0068	88	2p <sup>2</sup> 3s <sup>2</sup> D <sub>3/2</sub>	177.0925	177.0925	177.0925	156	2s2p4f <sup>4</sup> F <sub>9/2</sub>	217.7466		217.7466
21	2s <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	163.2112	163.2112	163.0068	89	2p <sup>2</sup> 3p <sup>4</sup> F <sub>7/2</sub>	177.2838	177.2838	177.2838	157	2s2p4f <sup>2</sup> D <sub>5/2</sub>	217.7894		217.7894
22	2s <sup>2</sup> 3d <sup>2</sup> P <sub>1/2</sub>	163.2112	163.2112	163.0068	90	2p <sup>2</sup> 3d <sup>4</sup> P <sub>3/2</sub>	177.3783	177.3783	177.3783	158	2s2p4f <sup>2</sup> G <sub>7/2</sub>	217.8182		217.8182
23	2s <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	163.2112	163.2112	163.0068	91	2p <sup>2</sup> 3d <sup>4</sup> F <sub>5/2</sub>	177.8569	177.8569	177.8569	159	2s2p4s <sup>4</sup> P <sub>5/2</sub>	218.2805		218.2805
24	2s2p3p <sup>4</sup> D <sub>1/2</sub>	163.2112	163.2112	163.0068	92	2p <sup>2</sup> 3d <sup>4</sup> D <sub>1/2</sub>	177.8905	177.8905	177.8905	160	2s2p4s <sup>2</sup> P <sub>3/2</sub>	218.5739		218.5739
25	2s2p3p <sup>4</sup> D <sub>3/2</sub>	163.2112	163.2112	163.0068	93	2p <sup>2</sup> 3s <sup>2</sup> P <sub>3/2</sub>	177.9252	177.9252	177.9252	161	2s2p4p <sup>4</sup> P <sub>3/2</sub>	219.3617		219.3617
26	2s2p3p <sup>4</sup> S <sub>3/2</sub>	163.2112	163.2112	163.0068	94	2p <sup>2</sup> 3p <sup>4</sup> P <sub>1/2</sub>	177.9925	177.9925	177.9925	162	2s2p4p <sup>4</sup> P <sub>5/2</sub>	219.4165		219.4165
27	2s2p3p <sup>4</sup> P <sub>1/2</sub>	163.2112	163.2112	163.0068	95	2p <sup>2</sup> 3p <sup>4</sup> D <sub>7/2</sub>	177.7014	177.7014	177.7014	163	2s2p4p <sup>2</sup> D <sub>7/2</sub>	219.6924		219.6924
28	2s2p3s <sup>4</sup> P <sub>5/2</sub>	163.2112	163.2112	163.0068	96	2p <sup>2</sup> 3d <sup>4</sup> P <sub>5/2</sub>	177.8569	177.8569	177.8569	164	2s2p4p <sup>2</sup> P <sub>3/2</sub>	219.8072		219.8072
29	2s2p3p <sup>2</sup> P <sub>1/2</sub>	163.2112	163.2112	163.0068	97	2p <sup>2</sup> 3d <sup>4</sup> D <sub>5/2</sub>	177.8905	177.8905	177.8905	165	2s2p4p <sup>2</sup> D <sub>5/2</sub>	220.0000		220.0000
30	2s2p3p <sup>2</sup> D <sub>5/2</sub>	163.2112	163.2112	163.0068	98	2p <sup>2</sup> 3d <sup>4</sup> F <sub>9/2</sub>	178.1044	178.1044	178.1044	166	2s2p4p <sup>2</sup> S <sub>1/2</sub>	220.1217		220.1217
31	2s2p3p <sup>2</sup> D <sub>3/2</sub>	163.2112	163.2112	163.0068	99	2p <sup>2</sup> 3d <sup>4</sup> D <sub>5/2</sub>	178.5144	178.5144	178.5144	167	2s2p4d <sup>4</sup> F <sub>9/2</sub>	220.5868		220.5868
32	2s2p3s <sup>2</sup> P <sub>3/2</sub>	164.1521	164.4218	164.4218	100	2p <sup>2</sup> 3d <sup>4</sup> P <sub>3/2</sub>	178.6582	178.6582	178.6582	168	2s2p4d <sup>4</sup> D <sub>5/2</sub>	220.6171		220.6171
33	2s2p3d <sup>4</sup> F <sub>3/2</sub>	164.8609	164.4521	164.4521	101	2p <sup>2</sup> 3d <sup>4</sup> P <sub>1/2</sub>	178.7642	178.7642	178.7642	169	2s2p4d <sup>4</sup> P <sub>3/2</sub>	220.6221		220.6221
34	2s2p3d <sup>4</sup> F <sub>5/2</sub>	165.4206	164.9840	164.9840	102	2p <sup>2</sup> 3d <sup>2</sup> G <sub>7/2</sub>	179.1552	179.1552	179.1552	170	2s2p4d <sup>4</sup> P <sub>1/2</sub>	220.6604		220.6604
35	2s2p3d <sup>4</sup> P <sub>5/2</sub>	165.9686	165.5013	165.5013	103	2p <sup>2</sup> 3d <sup>2</sup> P <sub>1/2</sub>	179.1603	179.1603	179.1603	171	2s2p4d <sup>4</sup> P <sub>3/2</sub>	220.6734		220.6734
36	2s2p3d <sup>4</sup> D <sub>3/2</sub>	166.2133	165.7409	165.7409	104	2p <sup>2</sup> 3d <sup>2</sup> D <sub>5/2</sub>	179.1977	179.1977	179.1977	172	2s2p4d <sup>2</sup> D <sub>5/2</sub>	220.8715		220.8715
37	2s2p3d <sup>4</sup> D <sub>1/2</sub>	166.2538	165.7826	165.7826	105	2p <sup>2</sup> 3p <sup>2</sup> D <sub>3/2</sub>	179.3160	179.3160	179.3160	173	2s2p4d <sup>2</sup> P <sub>3/2</sub>	220.9922		220.9922
38	2s2p3d <sup>4</sup> F <sub>7/2</sub>	166.2880	166.2880	166.2880	106	2p <sup>2</sup> 3d <sup>2</sup> D <sub>3/2</sub>	179.3255	179.3255	179.3255	174	2s2p4d <sup>2</sup> F <sub>7/2</sub>	221.0962		221.0962
39	2s2p3p <sup>4</sup> P <sub>3/2</sub>	166.3614	166.2384	166.2384	107	2p <sup>2</sup> 3s <sup>2</sup> S <sub>1/2</sub>	179.5545	179.5545	179.5545	175	2s2p4d <sup>2</sup> P <sub>1/2</sub>	221.2045		221.2045
40	2s2p3p <sup>4</sup> P <sub>5/2</sub>	166.5788	166.4449	166.4449	108	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	179.5798	179.5798	179.5798	176	2s2p4f <sup>4</sup> F <sub>7/2</sub>	221.2142		221.2142
41	2s2p3d <sup>2</sup> D <sub>3/2</sub>	167.1090	166.9380	166.9380	109	2p <sup>2</sup> 3p <sup>2</sup> D <sub>5/2</sub>	179.8585	179.8585	179.8585	177	2s2p4f <sup>4</sup> G <sub>9/2</sub>	221.2379		221.2379
42	2s2p3p <sup>4</sup> D <sub>7/2</sub>	167.1417	166.6575	166.6575	110	2p <sup>2</sup> 3p <sup>2</sup> F <sub>7/2</sub>	179.9614	179.9614	179.9614	178	2s2p4f <sup>4</sup> P <sub>3/2</sub>	221.2520		221.2520
43	2s2p3d <sup>2</sup> F <sub>5/2</sub>	167.2047	167.1139	167.1139	111	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	180.0236	180.0236	180.0236	179	2s2p4f <sup>4</sup> D <sub>3/2</sub>	221.2916		221.2916
44	2s2p3s <sup>2</sup> P <sub>1/2</sub>	167.3422	167.2395	167.2395	112	2p <sup>2</sup> 3p <sup>2</sup> P <sub>3/2</sub>	181.6660	181.6660	181.6660	180	2s2p4f <sup>2</sup> F <sub>7/2</sub>	221.3237		221.3237
45	2s2p3p <sup>2</sup> P <sub>3/2</sub>	167.3538	167.2602	167.2602	113	2p <sup>2</sup> 3p <sup>2</sup> P <sub>1/2</sub>	181.9045	181.9045	181.9045	181	2s2p4f <sup>2</sup> G <sub>11/2</sub>	221.3333		221.3333
46	2s2p3s <sup>2</sup> P <sub>3/2</sub>	167.9892	167.9185	167.9185	114	2p <sup>2</sup> 3d <sup>2</sup> F <sub>7/2</sub>	182.0481	182.0481	182.0481	182	2s2p4f <sup>4</sup> D <sub>1/2</sub>	221.3349		221.3349
47	2s2p3p <sup>2</sup> D <sub>5/2</sub>				115	2p <sup>2</sup> 3d <sup>2</sup> G <sub>9/2</sub>	182.2235	182.2235	182.2235	183	2s2p4f <sup>2</sup> G <sub>9/2</sub>	221.3642		221.3642

Notes. <sup>(a)</sup> GRASP calculation with QED-correction from the work of Aggarwal et al. (2008).



**Fig. 1.** Comparison of line strengths ( $S$ ) of electric-dipole transitions for ions spanning the sequence. For  $\text{Ne}^{5+}$ , MGB01 corresponds to the MCHF calculation of Mitnik et al. (2001) for transitions among the lowest 20 levels, while “up-triangle” symbols correspond to the data from the MCHF/MCDF collection<sup>6</sup>. For  $\text{Ar}^{13+}$ , comparisons are made with the GRASP calculation by Aggarwal et al. (2005) and with the AUTOSTRUCTURE calculation by Ludlow et al. (2010, hereafter LBL10) for all transitions amongst levels of the  $n = 2$  configurations. The “x” symbols denote transitions among the lowest 20 levels. For  $\text{Fe}^{21+}$ , a comparison is made with the MCDF calculation (Jonasuskas et al. 2006) and that of Badnell et al. (2001, hereafter BGM01) for all transitions amongst levels of the  $n = 2$  configurations. The “x” symbols are the same as for  $\text{Ar}^{13+}$ . For  $\text{Kr}^{31+}$ , we compare with the GRASP calculation by Aggarwal et al. (2008). The horizontal dashed lines correspond to an agreement within 20%.

The present AS calculation agrees well with the GRASP calculation, to within 1%, and even better than 0.5% for most levels, see Table 3. In the work of Ludlow et al. (2010)<sup>4</sup>, the orbital scaling parameters were adjusted by hand to bring the calculated  $n = 2$  level energies into close agreement with the NIST v4 experimental values. But our ab initio results agree much better with the NIST values for the  $n = 3$  and 4 levels. For compactness, we do not present their results in Table 3. We do note that the Ludlow et al. (2010) *R*-matrix calculations covered the whole argon isonuclear sequence and so they were constrained to use a simplified structure. With an isoelectronic sequence, once we have determined the best approach to the structure for one ion, the same one works with little change for every other one of the sequence (excluding near neutral).

For  $\text{Fe}^{21+}$ , Jonasuskas et al. (2006) performed an unprecedented large-scale calculation using the multi-configuration Dirac-Fock (MCDF) approach with the promotion of one, two, and three electrons from  $n = 2$  to all possible combinations of one, two, or three electrons in the shells up to  $n = 3$ . The present AS level energies agree within 0.5% for all levels of  $n = 3$  and 4 configurations. For low-lying levels of  $n = 2$  complex, the difference is still within 2%, see Table 4. Badnell et al. (2001) performed a similar calculation to the present one, but without inclusion of  $2s3l3l'$  and  $2p3s3l$  configurations, again using the

AUTOSTRUCTURE code<sup>5</sup>. Their resulting level energies show an excellent agreement with the present ones. Due to the similarity of the two approaches, their results are not listed in Table 4.

For the highly charged case of  $\text{Kr}^{31+}$ , the most recent theoretical work is the fully relativistic GRASP calculation performed by Aggarwal et al. (2008). Table 5 shows that the present AS calculation agrees to better than 1% with the GRASP calculation.

## 2.2. Structure: line strength $S$

Another test of our structure calculation is to compare line strengths ( $S_{ij}$  for a given  $i \leftarrow j$  transition). In terms of the transition energy  $E_{ji}$  (Ryd) for the  $j \rightarrow i$  transition, the absorption oscillator strength,  $f_{ij}$ , can be written as

$$f_{ij} = \frac{E_{ji}}{3g_i} S, \quad (1)$$

and the transition probability or Einstein’s  $A$ -coefficient,  $A_{ji}$ , as

$$A_{ji}(\text{au}) = \frac{1}{2} \alpha^3 \frac{g_i}{g_j} E_{ji}^2 f_{ij}, \quad (2)$$

where  $\alpha$  is the fine structure constant, and  $g_i, g_j$  are the statistical weight factors of the initial and final states, respectively.

Figure 1 illustrates a graphical comparison of line strengths with previous calculations for electric-dipole transitions for the four representative ions. For the lower charged  $\text{Ne}^{5+}$  ion, 76%

<sup>4</sup> Ballance provided us with their results for  $\text{Ar}^{13+}$  in the adf04 file format (priv. comm.).

<sup>5</sup> Their resulting data are available from the Open-ADAS database in the adf04 file format.

of all possible transitions among the lowest 20 levels agree with the MCHF calculation (Mitnik et al. 2001) to within 20%. Mitnik et al. (2001) demonstrated that the average difference is 24% between their results and the data from MCHF/MCDF collection database<sup>6</sup>. We illustrate this comparison again by “up-triangle” symbols in the top-left panel in Fig. 1, which reveals a comparable level of agreement with that in Table 2 of Mitnik et al. (2001).

For Ar<sup>13+</sup>, the 460-level GRASP calculation performed by Aggarwal et al. (2005) is the largest-scale work for this ion to our best knowledge. We provide a comparison with their results, again in Fig. 1. There are 63% of all electric-dipole transitions to levels of  $n = 2$  configurations which agree to within 20% between the two different calculations. For transitions among the lowest 20 levels, an even better (84%) agreement is found. The data from Ludlow et al. (2010) show a worse agreement with ours. There are only 32% of all available transitions to  $n = 2$  levels to agree within 20%. Even for transitions within  $n = 2$  levels, the percentage is 53%. Their lack of an optimized structure is likely the cause. Additionally, their radiative decay rate ( $A_{ij}$ ) values in adf04 file were scaled according the theoretical and NIST level energies. That might also contribute to some of the low percentage in the differences of dipole line strengths.

For Fe<sup>21+</sup>, the work of Jonauskas et al. (2006) is likely the largest-scale calculation. The present AS calculation agrees with their results to within 20% for 79% of all electric-dipole transitions to levels of  $n = 2$  complex. In comparison with the results of Badnell et al. (2001), 85% of all electric-dipole transitions to  $n = 2$  levels agree within 20%. This difference is attributed to the CI effect from the  $2s3l3l'$  and  $2p3s3l$  configurations included in our AS calculation.

For the highly charged case of Kr<sup>31+</sup>, a comparison is made with the GRASP calculation of Aggarwal et al. (2008). There are 64% of all transitions to levels of  $n = 2$  that agree to within 20%. For transitions within  $n = 2$  levels, the percentage is 92%.

The scatter plots show that the deviations between the present AS calculation and various previous results are much stronger and more widespread for the weaker transitions than the strong ones, as expected.

Overall, the atomic structure of the ions spanning the sequence is reliable, and the uncertainty in collision strengths ( $\Omega$ s) due to inaccuracies in the target structure is correspondingly small.

### 3. Scattering

The present parallel ICFT  $R$ -matrix calculations employed 40 continuum basis orbitals per angular momentum to represent the  $(N + 1)$ th-electron over the sequence. All partial waves from  $J = 0$  to 41 were included explicitly and the contribution from higher  $J$ -values was included using a “top-up” procedure (Burgess 1974; Badnell & Griffin 2001). The contribution from partial waves up to  $J = 12$  included electron exchange while those from  $J = 13$  to 41 were non-exchange, calculated using the exchange  $R$ -matrix code in its non-exchange mode. For the exchange calculation, a fine energy mesh was used to resolve the majority of narrow resonances below the highest excitation threshold, which has been tested to be sufficient for the convergence of the effective collision strength, see Fig. 2. From just above the highest threshold excitation to a maximum energy of ten times the ionization potential for each ion, a coarse energy mesh ( $1.0 \times 10^{-3} z^2$  Ryd, where  $z = Z - 5$  is the residual charge

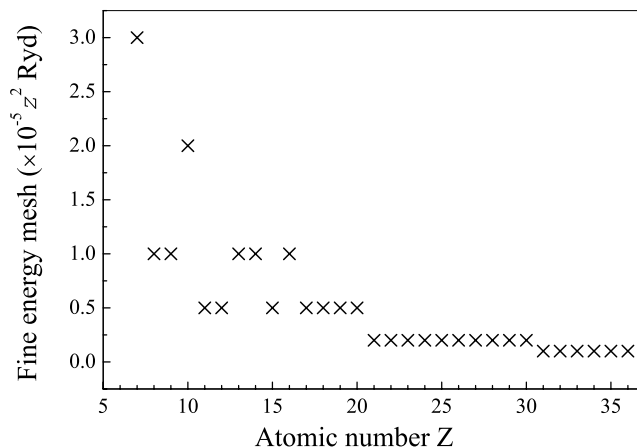


Fig. 2. Fine energy mesh employed in the outer region (exchange)  $R$ -matrix calculation for each ion.

of ion) was employed. For the non-exchange calculation, a step of  $1.0 \times 10^{-3} z^2$  Ryd was used over the entire energy range. Additionally, experimentally determined energies or adjusted energies were employed in the MQDT expressions used by the ICFT method to further improve the accuracy of the results, as was done for highly charged sulphur ions (Liang et al. 2011). The lowest-lying 8 LS terms (15 IC levels) of the  $n = 2$  complex were corrected for almost all ions over the iso-electronic sequence, as explained in detail in the structure section.

As mentioned in the introduction, we wish to determine excitation data for the 204 CC levels of the  $2s^x 2p^y$  ( $x + y = 3$ ),  $2s^2\{3, 4\}l$ ,  $2s2p\{3, 4\}l$ , and  $2p^2 3l$  configurations. But for some ions, these do not correspond to the lowest energy 204 levels (92 LS terms). When this occurs, we include additional terms in the close-coupling expansion so that all  $2p^2 3l$  levels are still in the close-coupling expansion and there are no “gaps” below them. For example, for N<sup>2+</sup> and O<sup>3+</sup>, the  $2p^2 4s$   $^4P/2P$ ,  $2p^2 4p$   $^2S/4P/4D$  terms were included.

To take the contribution from higher electron energies to high temperature effective collision strengths into account, the infinite energy Born limits (non-dipole allowed) and line strengths (dipole allowed) from AUTOSTRUCTURE were used to obtain collision strengths ( $\Omega$ ) at higher energies according to the procedure defined by Burgess & Tully (1992). The effective collision strengths at 13 electron temperatures ranging from  $2 \times 10^2 (z + 1)^2$  K to  $2 \times 10^6 (z + 1)^2$  K are produced as the end product with ADAS adf04 format (Summers 2004).

## 4. Results and discussions

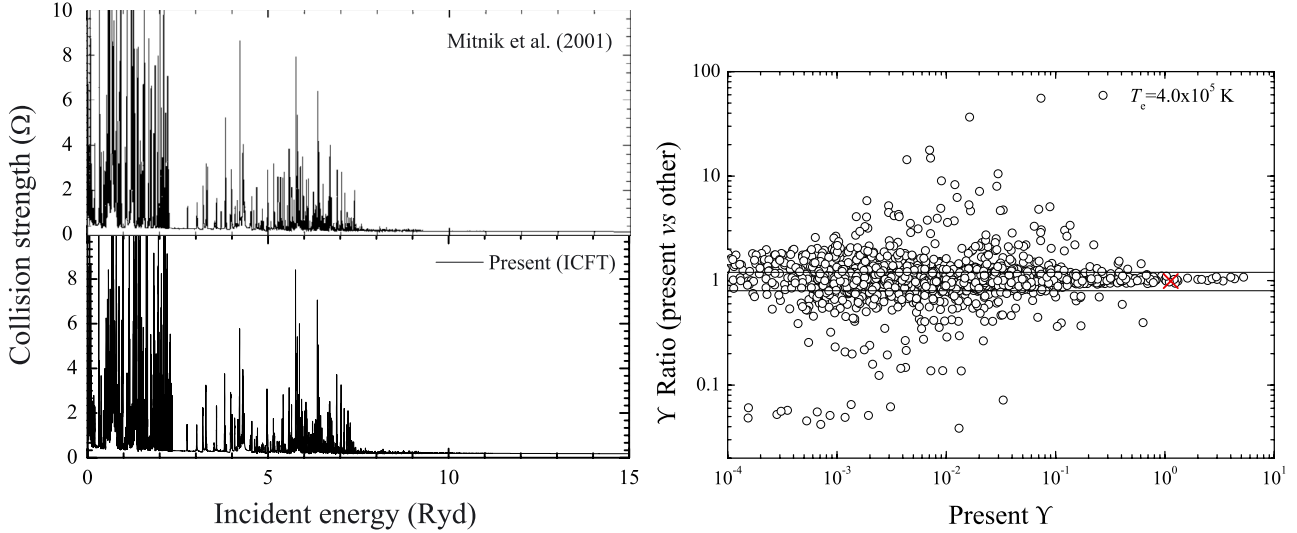
### 4.1. Comparison with previous calculations

As in our other iso-electronic sequence work, we selected several transitions to test the original collision strength for four ions (Ne<sup>5+</sup>, Ar<sup>13+</sup>, Fe<sup>21+</sup> and Kr<sup>31+</sup>) spanning over the sequence. An extensive comparison for effective collision strength will be given by a scatter plot to test how far the reliability reaches.

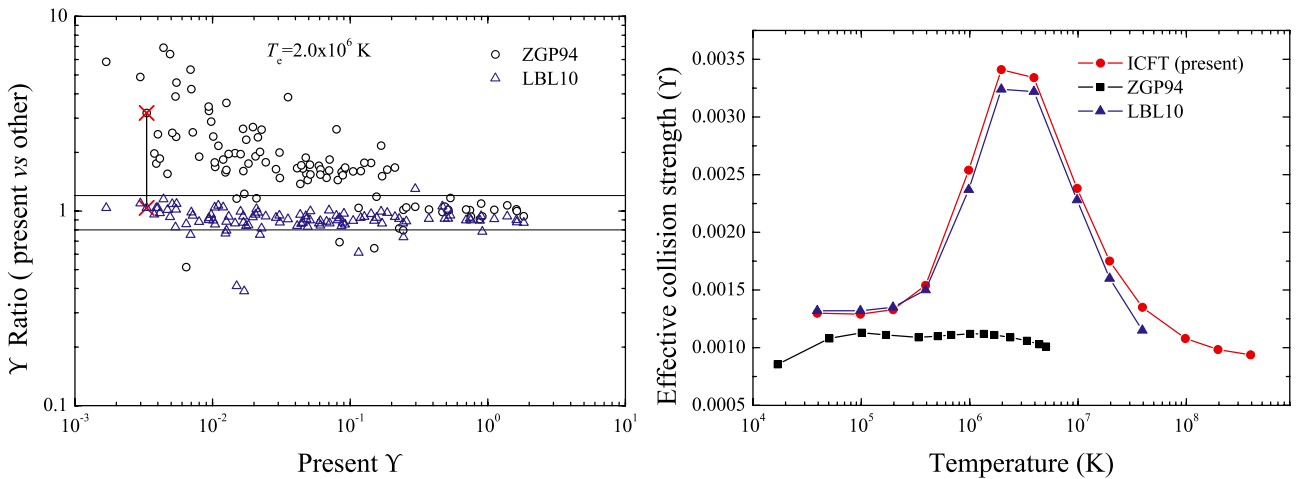
- Ne<sup>5+</sup> Mitnik et al. (2001) performed a 180-level ICFT  $R$ -matrix calculation for this ion with the same CC expansion as we did except for the  $2s2p4f$  configuration. As mentioned above, the MCHF approach was used to describe the target structure and three pseudo-orbitals were included to partially correct spectroscopic orbitals in this previous calculation. Our 204-level collision strength shows an excellent

<sup>6</sup> <http://nlte.nist.gov/MCHF/view.html>





**Fig. 3.** (Effective) collision strengths for  $\text{Ne}^{5+}$ . *Left*: excitation from the  $2s^22p^2P_{1/2}$  ground level to the  $2s^22p^2P_{3/2}$  level (1–2). *Right*: excitations amongst all 15 levels of the  $n = 2$  configurations at the temperature ( $T_e = 4.0 \times 10^5$  K) of peak fractional abundance in ionization equilibrium. The (red) “x” marks the 1–2 excitation shown in the lefthand panel. Double-horizontal lines correspond to agreement within 20%. *Notes*: the collision strength of Mitnik et al. (2001) is a scanned picture.



**Fig. 4.** Comparison of effective collision strengths for  $\text{Ar}^{13+}$ . *Left*: all excitations among the 15 levels of the  $n = 2$  configurations at the temperature ( $T_e = 4.0 \times 10^6$  K) of peak fractional abundance in ionization equilibrium. The “x” symbol corresponds to the  $2s^22p^2P_{3/2}-2p^3^2P_{3/2}$  (1–15) excitation shown in the righthand panel, which is linked for the two different previous calculations. Double-horizontal lines correspond to agreement within 20%. *Right*: the effective collision strength of the 1–15 transition as a function of temperature (K). ZGP94 and LBL10 correspond to the Breit-Pauli *R*-matrix works of Zhang et al. (1994) and Ludlow et al. (2010), respectively.

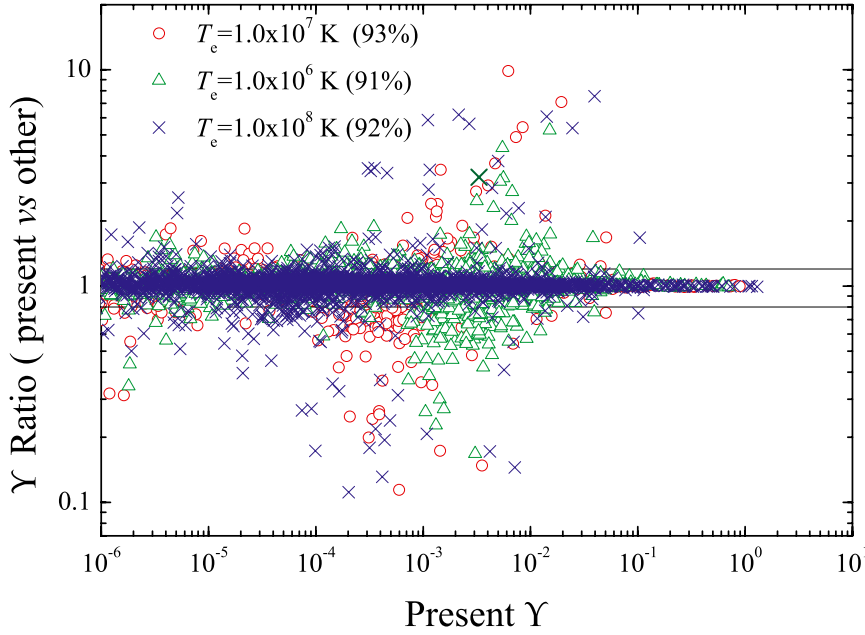
agreement with this previous one, see left panel in Fig 3. An extensive comparison of effective collision strength is given in the right panel of Fig. 3 for all excitations from levels of  $n = 2$  configurations at a temperature of peak fraction in ionization equilibrium. About 73% of the excitations agree within 20%.

- $\text{Ar}^{13+}$  The small-scale ( $n = 2$ ) *R*-matrix calculation performed by Zhang et al. (1994) is extensively adopted by various databases, e.g. Open-ADAS<sup>7</sup> and Chianti v7 (Landi et al. 2012). Comparison with these data for all excitations among the 15 lowest-lying levels reveals that the previous *R*-matrix data are systematically lower than ours, and the deviations are stronger for weaker excitations, see Fig. 4. However, the data from the work of Ludlow et al. (2010) agree well

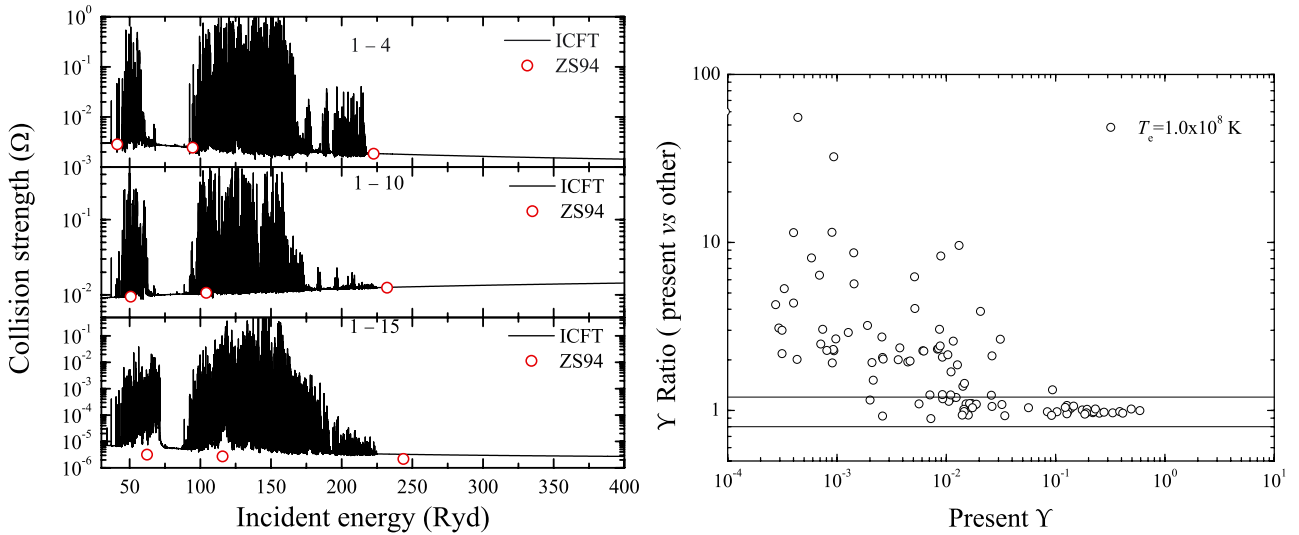
with ours even though only 36 IC levels of  $(1s^2)2s^x2p^y$  ( $x + y = 3$ ),  $2s^2\{3, 4, 5\}l$  configurations were included in their close-coupling expansion. Ninety percent of all transitions within  $n = 2$  levels agree to within 20%. For the  $2s^22p^2P_{3/2}-2p^3^2P_{3/2}$  (1–15) excitation, there is an obvious bump in the present ICFT *R*-matrix calculation at temperatures of  $10^6-10^7$  K, with the difference being up to  $\sim 3.5$  when compared with Zhang et al.’s data. This is an obvious enhancement due to resonances attached to  $n = 3$  that were not included in the previous small-scale calculation. The good agreement with Ludlow et al.’s data also supports this.

- $\text{Fe}^{21+}$  After carrying out a level mapping procedure according to  $LSJ^\pi$  and configurations, an extensive comparison was made with a previous (204-level) ICFT *R*-matrix calculation (Badnell et al. 2001) at three temperatures of  $10^5$ ,  $10^6$ , and

<sup>7</sup> <http://open.adas.ac.uk/>



**Fig. 5.** Comparison of effective collision strength with the results of Badnell et al. (2001) for  $\text{Fe}^{21+}$  for all excitations from the lowest 15 levels at temperatures of  $T_e = 1.0 \times 10^6, 10^7$  and  $10^8$  K. Double-horizontal lines correspond to agreement within 20%.



**Fig. 6.** (Effective) collision strengths for  $\text{Kr}^{21+}$ . *Left:* present collision strengths for  $2s^2 2p^2 P_{1/2} - 2s 2p^2 \ ^4P_{3/2}$  (1–4),  $2s^2 2p^2 P_{1/2} - 2s 2p^2 \ ^2P_{3/2}$  (1–10), and  $2s^2 2p^2 P_{1/2} - 2p^3 \ ^2P_{3/2}$  (1–15) transitions along with the distorted-wave calculation by Zhang & Sampson (1994a, ZS94). *Right:* ratio of effective collision strength between the present ICFT  $R$ -matrix calculation and DW results available from the Open-ADAS database<sup>7</sup> at a temperature of  $1.0 \times 10^8$  K. Double-horizontal lines correspond to agreement within 20%.

$10^7$  K. Almost all excitations (93%) agree to within 20% for the two different calculations with a different target structure, see Fig. 5. The differences between them and the widespread agreement do not change much with increasing temperature. This results from the consistent resonance structure in the two calculations. Badnell et al. (2001) made a detailed assessment for their calculation with previous available data, therefore we will not repeat the comparison here.

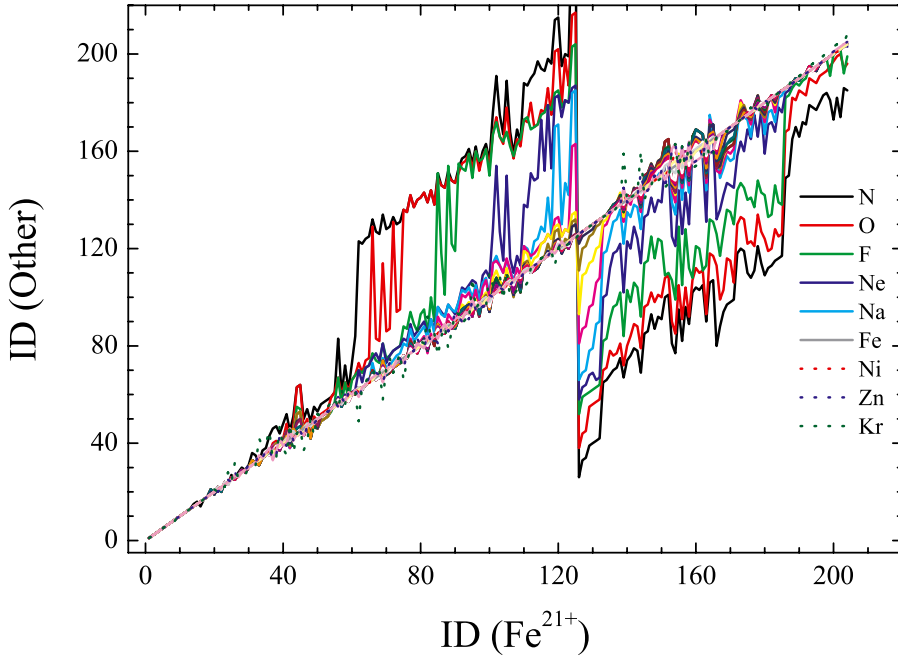
–  $\text{Kr}^{31+}$  To our best knowledge, there are no  $R$ -matrix excitation data available for this ion. Therefore, we compared the background of the present ICFT  $R$ -matrix calculation with that from a distorted-wave calculation performed by Zhang & Sampson (1994a,b) for excitations from the ground level  $2s^2 2p^2 P_{1/2}$ . Figure 6 illustrates some excitations from this comparison. The background of the collision strengths agrees well with the DW calculation. As expected,

the present effective collision strengths  $\Upsilon$  are systematically higher than those from the distorted-wave approach due to the inclusion of resonances.

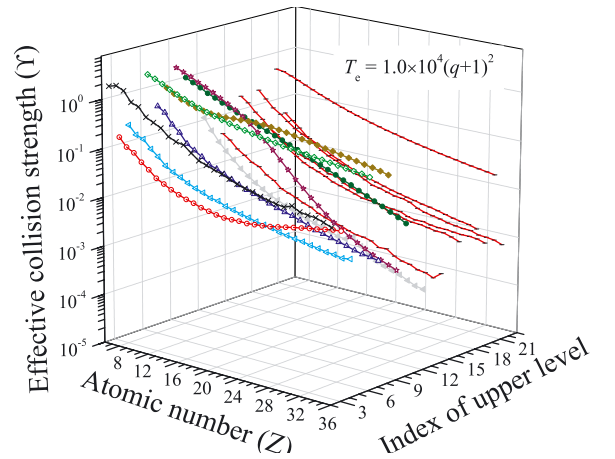
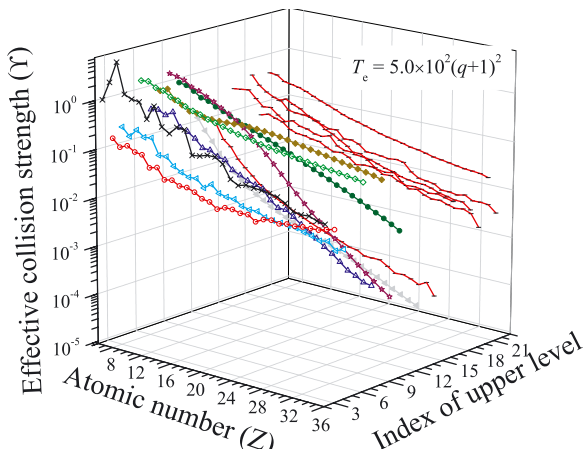
From the above comparison for the four specified ions ( $\text{Ne}^{5+}$ ,  $\text{Ar}^{13+}$ ,  $\text{Fe}^{21+}$  and  $\text{Kr}^{31+}$ ) spanning the iso-electronic sequence, we believe the present ICFT  $R$ -matrix results ( $\Omega$  and  $\Upsilon$ ) to be reliable. For ions near neutral (below  $\text{O}^{3+}$ ),  $R$ -matrix with pseudostates calculations are needed to consider ionization loss in the excitation, but ours are the best data available to date.

#### 4.2. Trends of iso-electronic sequence

As in our previous sequence works (Witthoef et al. 2007; Liang et al. 2009c, 2010, 2011), we take configuration, total angular



**Fig. 7.** Level ordering with the original level index (ID) relative to the ordering of  $\text{Fe}^{21+}$  by mapping according to the “good” quantum numbers – configuration, total angular momentum  $J$ , and energy ordering for ions spanning the entire sequence. The spikes and dips are due to the shift of a given level, for example,  $2p^2 3s \ ^4P$  (62–65) levels in  $\text{Fe}^{21+}$  move to levels above 120 in  $\text{N}^{2+}$ .



**Fig. 8.** Effective collision strength ( $\Upsilon$ ) for excitations from the ground level to all 22 lowest-lying excited levels at temperatures of  $T_e = 5 \times 10^2 (q+1)^2$  and  $1 \times 10^4 (q+1)^2$  K (here  $q = Z - 5$ ) along the iso-electronic sequence. *Notes:* the index number refers to the ID number in the reference ion – Fe.

momentum  $J$ , and energy ordering as a good quantum number for level matching in the comparison between different calculations and the investigation of  $\Upsilon$  along the iso-electronic sequence, see Fig. 7. This satisfactorily eliminates uncertainty originating from the non-continuity of level-ordering along the sequence. We used Fe as the arbitrary reference ion for the level-ordering.

In Fig. 8, we show the effective collision strength  $\Upsilon$  at temperatures of  $T_e/(q+1)^2 = 5 \times 10^2$  and  $10^4$  K along the iso-electronic sequence for excitations from the ground level to the lowest-lying (in  $\text{Fe}^{21+}$ ) 22 excited levels. At the low temperature of  $5 \times 10^2 (q+1)^2$  K, spikes and/or dips are observed at low charges for some transitions, e.g.  $2s^2 2p \ ^2P_{1/2} \rightarrow 2s^2 2p \ ^2P_{3/2}$  (1–2). With increasing threshold energy, that is to higher excited levels, this irregularity becomes weaker and eventually disappears. At the high temperature of  $1 \times 10^4 (q+1)^2$  K, the spikes and/or dips disappear, as expected, because the resonance contribution becomes weaker and eventually negligible.

## 5. Summary

We have performed 204-level ICFT *R*-matrix calculations for the electron-impact excitation of all ions of the boron-like iso-electronic sequence from  $\text{C}^+$  to  $\text{Kr}^{31+}$ .

Good agreement with the available experimentally derived data and the results of others for level energies and line strengths  $S$  for several specific ions ( $\text{Ne}^{5+}$ ,  $\text{Ar}^{13+}$ ,  $\text{Fe}^{21+}$ , and  $\text{Kr}^{31+}$ ) spanning the iso-electronic sequence, supports the reliability of our *R*-matrix excitation data. This was confirmed specifically by detailed comparisons of  $\Omega$  and/or  $\Upsilon$  with previous *R*-matrix calculations, where available, for the four specific reference ions.

Our *R*-matrix excitation data are expected to be an important improvement on the current data (from relativistic distorted-wave approach), which are extensively used by the spectroscopic diagnostic modelling communities in astrophysics and magnetic fusion.

By excluding the level-crossing effects on the  $\Upsilon$ , we examined the iso-electronic trends of the effective collision strengths. As expected, a complicated pattern of spikes and dips of  $\Upsilon$  at low temperatures was noted again along the sequence as shown in our other series works.

The data are made available in the ADAS *adf04* format (Summers 2004) at the archives of the APAP<sup>2</sup>, OPEN-ADAS<sup>7</sup> and will be included in the CHIANTI<sup>8</sup> database. At the APAP-network website<sup>2</sup>, the original collision strength also can be made available.

In conclusion, we have generated an extensive set of reliable excitation data with the ICFT *R*-matrix method for spectroscopy/diagnostic research within the astrophysical and fusion communities. This will replace the data from DW and small-scale *R*-matrix calculations presently used by these communities, and it is expected to identify new lines and may overcome some shortcomings in present astrophysical modelling.

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<sup>8</sup> <http://www.chianti.rl.ac.uk/>