

At-line validation of Optical Coherence Tomography as in-line/at-line Coating Thickness Measurement Method

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ABSTRACT

Optical Coherence Tomography (OCT) is a promising technology for monitoring of pharmaceutical coating processes. However, the pharmaceutical development and manufacturing require a periodic validation of the sensor's accuracy. For this purpose, we propose polyethylene terephthalate (PET) films as a model system, which can be periodically measured during manufacturing coating monitoring via OCT. This study proposes a new approach addressing the method validation requirement in the pharmaceutical industry and presents results for complementary methods. The methods investigated include direct measurement of the layer thickness using a micrometer gauge as reference, X-ray micro computed tomography, transmission and reflectance terahertz pulsed imaging, as well as 1D- and 3D-OCT. To quantify the significance of OCT for pharmaceutical coatings, we compared the OCT results for commercial Thrombo-ASS and Pantoloc tablets with direct measurements of coating thickness via light microscopy of microtome cuts. The results of both methods correlate very well, indicating high intra- and inter-tablet variations in the coating thickness for the commercial tablets. The light microscopy average measured coating thickness of Thrombo-ASS (Pantoloc) was 71.0 μm (83.7 μm), with an inter-coating variability of 8.7 μm (6.5 μm) and an intra-coating variability of 2.3 μm to 9.4 μm (2.1 μm to 6.7 μm).

Keywords (4-6): optical coherence tomography (OCT); terahertz pulsed imaging (TPI); micro computed tomography (μCT); reference material; coating thickness variability

1. INTRODUCTION

In the last 28 years optical coherence tomography (OCT) has become an established standard technology in medicine and the clinical practice (de Boer et al., 2017). Apart from medical applications, OCT can provide valuable insights into various structured materials when non-destructive testing is required (Nemeth et al., 2013). In 2009, Mauritz et al. demonstrated first attempts to investigate pharmaceutical coatings by means of OCT (Mauritz et al., 2010), opening a new field of applications for this technology. In the years after, several research groups, including our own, have demonstrated that OCT is a very promising technology for non-destructive monitoring of pharmaceutical film coating

39 processes (Lin et al., 2018) for tablets (Koller et al., 2011; Lin et al., 2015; Markl et al., 2015a, 2014)
40 and pellets (Li et al., 2014; Markl et al., 2015b). The literature indicates that OCT can provide
41 information about critical material attributes, such as coating thickness, inner structure and
42 homogeneity (intra- and inter-coating variability) of pharmaceutical coatings applied to tablets (Dong
43 et al., 2017; Lin et al., 2017; Markl et al., 2018) and pellets (Li et al., 2014; Wolfgang et al., 2019). As a
44 direct measurement technique, OCT does not require the development and maintenance of
45 chemometric models for data interpretation, as is typically the case for near-infrared (Möltgen et al.,
46 2013; Wahl et al., 2019) or Raman spectroscopy (Barimani and Kleinebudde, 2017; Müller et al., 2010).
47 In contrast to more established spectroscopic approaches, OCT can reference the measured signals to
48 known spectral distances and natural constants (speed of light). The only material-dependent variable
49 is the refractive index of the materials tested. With a high axial resolution of a few microns and a
50 scanning speed of up to 250 kHz, OCT makes it possible to characterize coating structures within
51 microseconds.

52 Besides medical and pharmaceutical applications, low coherence interferometry (upon which OCT is
53 based) can be used to measure coating thickness (Kühnhold et al., 2015; Manallah et al., 2015) and
54 optical properties of polymer films, such as topography (Ghim et al., 2013), roughness (Yoshino et al.,
55 2017) and refractive indices (Yen et al., 2014). Also inline monitoring of coating process applications in
56 industrial coaters (both for tablets and pellets) have been demonstrated (Sacher et al., 2019).
57 Nevertheless, before introducing industrial OCT systems into the pharmaceutical industry, it is critical
58 to demonstrate that the measurements are reproducible and accurate. This is required by Good
59 Manufacturing Practice (GMP) requirements. Surprisingly, to the best of the authors' knowledge, there
60 is no commonly available or conventional standard reference material that can be readily used to
61 validate industrial OCT systems in terms of coating thickness measurements suitable for pharma
62 applications. There has been work published discussing the need for OCT depth calibration in the past.
63 Approaches range from precision laser-etched nanoparticles in polyurethane-resin (Gabriele Sandrian
64 et al., 2012), to photolithographic 3D printing, mimicking the commonly known USAF 1951 test chart
65 (Hu et al., 2014) in a three-dimensional way. Even highly sophisticated 3D printed eye phantoms
66 simulating human eyes with retinal features have been presented (Corcoran et al., 2015), but none of
67 them fulfils the requirements for an industrial OCT reference target.

68 Thus, the goal of this study was to identify reference materials suitable for pharmaceutical OCT
69 validation and to propose a possible solution by periodically validating the in-process OCT via
70 measurements of standardized films. Since Terahertz pulsed imaging (TPI) and OCT have been reported
71 to be complementary technologies with respect to pharmaceutical coating investigation (Zhong et al.,
72 2011), it would be additionally beneficial if the reference material would also be suitable for TPI. There
73 has been work presented for TPI where polymer foils aided as a reference (Zeitler et al., 2007). In
74 addition to identifying a suitable reference material, measurements of commercial tablets acquired
75 using a commercial pharma OCT system were validated to demonstrate that the OCT readings are
76 accurate and valid, as well as to illustrate the degree of coating thickness variation in the tablets.

77 **2. MATERIALS AND METHODS**

78 *2.2 Material Selection Considerations*

79 Currently, only one dedicated commercial OCT reference target is available. It is made of laser-
80 structured fused silica and manufactured and distributed by Arden Photonics. The Arden Photonics

81 reference target APL-OP01 (Arden Photonics Ltd., Solihull, United Kingdom) is intended to be a
82 reference and validation target for ultra-high resolution OCT (UHR-OCT) used in ophthalmic surgery. It
83 provides a reference for the point spread function, sensitivity, lateral resolution and distortion (Arden
84 Photonics Ltd, 2018), but not for the layer thickness that could be used for determining the coating
85 layer thicknesses. Unfortunately, the existing reference target is not suitable for validation of industrial
86 OCT equipment since its structures have a lateral linewidth of less than 2 μm (manufacturer's
87 specification). As such, the lines are too thin to be applied in an industrial OCT sensor whose lateral
88 resolution is typically within the range of 8-20 μm (in air). Additionally, several specific requirements
89 have to be taken into account when applying equipment in pharmaceutical manufacturing
90 environments, including the Good Manufacturing Practice (GMP) guidelines, hygiene design
91 guidelines, availability of material certificates (for FDA approval), resistance of used materials against
92 organic solvents, detergents, moisture, mechanical stress (e.g., glass breakage) and heat. Furthermore,
93 a suitable reference material for industrial validation of OCT equipment ideally has to have additional
94 optical properties, e.g., a refractive index similar to that of the materials tested, uniform optical
95 properties and a traceable quality.

96 After investigating several potential materials, such as the anodization layer of anodized aluminium
97 (not accurate enough in terms of reproducible thickness), several glasses (contamination of
98 pharmaceutical processes with glass fragments is a major issue that may have legal consequences) and
99 plastics, we found bi-axially oriented polyethylene terephthalate (PET) foils to be the most promising
100 one. The specific reasons for selecting it are its well-known physical properties and a refractive index
101 similar to that of dried pharmaceutical coatings. Moreover, no other materials with a suitable
102 refractive index, such as polypropylene (PP), polyamides (PA) and polyethylene-naphthalate (PEN),
103 were available within the desired range of thickness (3-300 μm).

104 *2.3 Biaxially Oriented Polyethylene Terephthalate Films (PET)*

105 PET appears to be a reference material suitable for OCT standards. The production process for PET
106 films has been carefully optimized to deliver highly reproducible products since one of its main
107 applications is the manufacturing of dielectric separation layers for capacitors. With that regard, a
108 reproducible and homogeneous film thickness is crucial since it directly affects the dielectric strength
109 and achievable specific capacitance. In addition, the constant and highly reproducible optical
110 properties of PET films, no water absorption, low thermal expansion coefficient and resistance to all
111 chemicals typically used in the pharmaceutical industry suggest that this material can be applied as an
112 OCT reference standard. Considering the effects of ageing, PET is a persistent material. What is a
113 drawback from an ecological point of view is an advantage for the expected shelf-life of PET foils as a
114 reference material. Studies to the accelerated degradation of PET (Bell, 2016) and the material
115 properties provided by the manufacturers indicate that under normal conditions the degradation is
116 neglectable, considering the material is stored at room temperature and constant humidity without
117 exposing it to UV radiation. Based on our investigations we would expect no altering of critical
118 properties for our intended use within years. In terms of mechanical stability the material is quite
119 resistant, nevertheless we put all foil samples in a sample holder to ensure that they are straight and
120 protected against damage. However, PET has one drawback: during the manufacturing process the
121 films become bi-axially stretched and birefringent (Amborski and Flierl, 1953). To account for this, the
122 PET-foils of a validation or calibration target should always be measured in the same orientation
123 relative to the OCT sensor. This was guaranteed by the use of the above mentioned foil holder.
124 Moreover, the birefringent behaviour is not a major problem for the intended use, because the

125 refractive indices in plane of PET foils are nearly the same (less than 0.002 deviation) and only the
126 index orthogonal to the foil plane deviates, guaranteeing reproducible measurements when using a
127 defined geometry during reference measurements along the plane.

128 The suitability of PET foils as a reference standard was examined based on experiments using the brand
129 product “Mylar A” manufactured by DuPont (Dupont Teijin Films, Dumfries, United Kingdom) with
130 nominal sheet thicknesses of 19, 36, 50, 75, 100, 125 and 190 μm . According to the manufacturer, the
131 films have a thickness tolerance of $\pm 5\%$ (based on weight). Characterization of the foils as a validation
132 target was carried out using several measurement technologies described below. The physical
133 properties of Mylar foils were previously summarized by DuPont (DuPont Teijin Films, 2003) and in
134 addition to the Mylar A foils, we investigated Hostaphan RN foils manufactured by Mitsubishi
135 (Mitsubishi Polyester Film GmbH, Wiesbaden, Germany). Since both materials are produced in the
136 same manner and reportedly have the same electrical and physical properties, they should have the
137 same behaviour when tested. For this additional set of samples the measurements were performed
138 only via OCT over an extended thicknesses range of 12-350 μm (12, 23, 50, 75, 100, 190 and 350 μm)
139 in order to establish if the materials are interchangeable as an OCT reference material. Based on the
140 combined measurements for both PET materials, we examined the linearity of results within the
141 desired thickness range.

142 It has been reported that biaxially stretched PET foils are prone to slight deviations in the refractive
143 index along the thickness-axis with an increasing thickness (Elman et al., 1998) as a result of the
144 manufacturing process. To that end, we tested both materials for their linearity throughout the entire
145 thickness range to determine if this is an issue for industrial OCT systems.

146 *2.4 Micrometer Gauge Measurements*

147 As a reference method, we carried out direct measurements of the foil sheets using a precision
148 micrometer gauge (Mitutoyo QuantumMike, MDE-25MJ, 0-25 mm) with a resolution of 1 μm ,
149 (Mitutoyo Europe, Neuss, Germany). The micrometer gauge utilises a torque-regulation mechanism to
150 maintain the contact pressure constant between the measurements. In order to study the
151 homogeneity of film thickness, between 111 and 134 measurements were taken in various positions
152 for each foil.

153 *2.5 X-Ray Micro Computed Tomography*

154 X-ray micro computed tomography ($X\mu\text{CT}$) measurements of films were performed using a Bruker
155 Skyscan 1172 (Bruker microCT, Kontich, Belgium). For this purpose, the films were stacked between
156 separating layers of ordinary copier paper sheets (80 g/m^2) and the entire stack was measured in a
157 single acquisition. The images were recorded with a voxel size of 1.49 μm and the layer thickness was
158 calculated based on the $X\mu\text{CT}$ images in ten positions for each foil.

159 *2.6 Terahertz Pulsed Imaging*

160 Terahertz time-domain measurements were performed using a TeraPulse 4000 (TeraView Ltd.,
161 Cambridge, United Kingdom). Transmission and reflection measurements were undertaken to infer
162 the refractive index and measure the foil thicknesses. Transmission measurements were acquired
163 under nitrogen gas purge. The reflectance measurements were accomplished using a fiber-coupled
164 probe head with a fixed angle of reflection of 30° . In all Terahertz measurements, the foils were

165 inclined at 7° relative to the terahertz beam in order to prevent multiple internal reflections that would
166 result in Fabry-Pérot resonance artefacts during the acquisition.

167 The refractive index for the Terahertz measurements was extracted from the transmission
168 measurements of foils with thickness of 100, 125 and 190 µm using the micrometer gauge
169 measurements as the reference method and was calculated to be 1.765 +/- 0.011. Based on this
170 refractive index, we estimated an axial resolution limit of ≈ 35 µm for measuring the thickness of films
171 via the Terahertz reflection method by directly resolving the time-of-flight peaks from two subsequent
172 reflections in the time-domain waveform. Since in the terahertz measurements only a single point on
173 each sample was measured, no standard deviations in the spatial thickness variation of each sample
174 were recorded.

175 *2.7 Optical Coherence Tomography*

176 OCT measurements were performed using two different OCT systems. To acquire full volume
177 information, an in-house 3D OCT prototype as described in (Markl et al., 2018) was used. Fully
178 automated 1D OCT measurements were carried out via a commercial pharma OCT system (OSeeT
179 Pharma 1D, Phyllon, Austria) equipped with exchangeable perforated rotating drums with an outer
180 diameter of 200 mm. In this setup it is possible to move samples (e.g., foils) mounted along the
181 circumference of the drum in front of a static 1D-OCT sensor in a reproducible manner at a pre-defined
182 speed or, alternatively, to mimic the behaviour of a moving tablet bed when the tablets are placed
183 inside the drum, with the sensor scanning the interior of the moving tablet bed through the
184 perforation. All measurements in the drum-setup were performed using the drum rotating at 35 rpm
185 to prevent artefacts due to various circumferential velocities.

186 Both OCT systems have a super luminescent diode as light-source with a central wavelength of 832 nm
187 and a spectral bandwidth of 75 nm, resulting in a theoretical axial resolution of 4.1 µm (in air, n = 1).
188 The chosen optical setup of the sensor head, as described in (Koller et al., 2011), results in a lateral
189 resolution of 10 µm in the 3D configuration. The lateral resolution of the commercial 1D-OCT system
190 is reported to be 14 µm based on the specifications of the system.

191 For all 3D-OCT measurements, the sensor exposure time was 30 µs and the idle time (for read-out and
192 digitalization) was 1.9 µs, which resulted in an acquisition rate of 31.3 kHz. The latter corresponds to
193 the number of single-depth scans (A-scans) per second, corresponding to a frame rate of 30.6 fps. All
194 measurements for foils and tablets were performed en-face. In 1D measurements, the sensor exposure
195 time was 4 µs and the idle time was 6 µs for read-out, digitization and evaluation, resulting in a real-
196 time capable framerate of 97.66 fps. All samples measured by the 1D system were inclined at 5° to
197 prevent multiple internal reflections that would otherwise result in Fabry-Pérot resonance artefacts
198 during the acquisition.

199 The refractive index for the PET foils was determined prior to the OCT measurements based on an
200 additional foil sample with a thickness of 50 µm, which was qualified according to ISO 534:2011-11 by
201 an external facility (Technical Testing and Research Institute for Paper, Pulp and Fibre Technology,
202 University of Technology, Graz, Austria). Based on the certified thickness and the pixel-distances in the
203 OCT images, the refractive index for the light source (central wavelength and spectral distribution) was
204 calculated based on 5 replicated volume measurements in various positions of the foil to be $n = 1.615$
205 ± 0.002 for Mylar and $n = 1.707 \pm 0.041$ for Hostaphan, respectively. These refractive indices were

206 used for all PET evaluations of the respective materials and lead to theoretical axial resolutions of
207 2.5 μm for Mylar and 2.4 μm for Hostaphan.

208 The refractive indices for the tablet coatings measured were calculated based on OCT cross-sectional
209 images of separate, additional tablet samples compared to microscopy images of the tablets in the
210 position where the OCT image was acquired. The refractive indices were calculated to be
211 $n = 1.48 \pm 0.02$ for the Thrombo ASS and $n = 1.45 \pm 0.02$ for the Pantoloc coating.

212 For the 3D OCT scans of PET-foils and for the tablets, the volumetric scans acquired were automatically
213 evaluated by calculating the mean thickness and variation based on 524,288 individual A-scans for each
214 sample. The scanned area of each sample was 3.12 mm x 3.12 mm in all measurements. Linearity
215 measurements for the two PET materials were performed based on additional 3D volumetric scans.

216 *2.8 Commercial Tablets Tested*

217 50 commercially-available tablets of Thrombo-ASS (100 mg acetylsalicylic acid, G.L. Pharma GmbH,
218 Lannach, Austria) and additional 50 tablets of Pantoloc (40 mg pantoprazole, Takeda Pharma GmbH,
219 Vienna, Austria), all coated with a clear enteric coating, were purchased at a local pharmacy. All sample
220 tablets were manually numbered on the tablet band using a fine liner (Staedler permanent Lumocolor,
221 blue) that is transparent at the wavelengths applied by both OCT systems. All tablets were individually
222 measured using the above-described 3D-OCT system, after which all tablets of one sample were
223 measured at once via the 1D-OCT system in the rotating drum setup. For this purpose the whole
224 sample was filled in the rotating drum, with the tablets moving free and randomly inside during
225 acquisition, as is the case in an in-line scenario. Speed was chosen to ensure a good mixing to avoid
226 acquisition of the same tablet parts during measurement. This was done to ensure the measurement
227 of different tablets at different positions to gain a good statistical basis. The sensor in this setup was
228 mounted outside the rotating drum scanning through the wholes inside the moving tablet bed.

229 Measurements via the in-house 3D OCT system were accomplished by recording cross-sectional
230 images (B-scans) of all tablets and performing a subsequent graphical evaluation of the recorded
231 images. For every B-Scan of the 3D measurements, the pixel distances between the top interface and
232 the coating core-interface were manually determined using the graphical software ImageJ. Starting
233 point for all evaluations was the centre of each B-scan with ten measurements in a distance of 100 μm
234 on both sides covering a length of 2 mm in total. The coating thicknesses were calculated taking into
235 account the corresponding refractive index. An automated evaluation of the 1D OCT measurements
236 was performed using the software "OSeeT Pharma 1D v 3.2.3" provided with the 1D OCT system.

237 *2.9 Microtome Cuts and Light Microscopy*

238 Subsequent to the OCT measurements, 11 of the Thrombo ASS and 10 of the Pantoloc tablets were
239 randomly chosen and examined off-line using light microscopy. The entire procedure was executed
240 externally at the Center for Electron Microscopy (Graz, Austria). Following the 3D OCT measurements,
241 all selected tablets were marked using a soft pencil (hardness 4B) to prevent damage to the tablet
242 surface. The marking was performed so that the OCT measurement position could be reconstructed
243 without affecting the position of the tablet surface where the OCT cross-sectional images were taken.
244 The ultimate goal was to examine the coating structure as close to this position as possible. Next, the
245 tablets were cut in half along the middle of the tablet band and both halves were embedded in epoxy
246 resin Epofix (Struers GmbH, Willich, Germany) to fix and stabilize them for the microtome cuts. The

247 resin was used to prevent mechanical and thermal stress to the samples, which potentially could result
 248 in changes to the structures. The fixation time was 12 hours.

249 Once the resin had cured the embedded tablet halves were pre-cut close to the mark with a scalpel
 250 and dry microtomed into progressively thinner slices until a smooth surface finish for the interface in
 251 the location of the OCT measurements was achieved. Microtome cuts were performed with a precision
 252 microtome (Leica UC6, Leica Microsystems GmbH, Wetzlar, Germany) and examined microscopically
 253 using a Zeiss Axioplan with Axiocam IcC1 (Carl Zeiss Microscopy GmbH, Jena, Germany) at a
 254 magnification of 50x with direct illumination. The first microtome cuts were accomplished with a glass
 255 knife (slices starting at 5 and down to 1 μm thickness) to protect the histological diamond blade, which
 256 was used for the final thinnest slices (300 to 100 nm slices). Following this procedure allowed us to
 257 minimize any cross-contamination by smearing and plastic deformation of the coating material,
 258 preserving the coating structure as much as possible during microtoming. During microscopy, no
 259 deformation or smearing of coatings was detected. During light microscopy examination, a minimum
 260 of seven measurements per microtome cross section (tablets 2, 5, 12, 23, 32, 44) was performed. The
 261 remaining tablets were measured in 18 individual positions that refer to the tablet cap area.

262 3. RESULTS

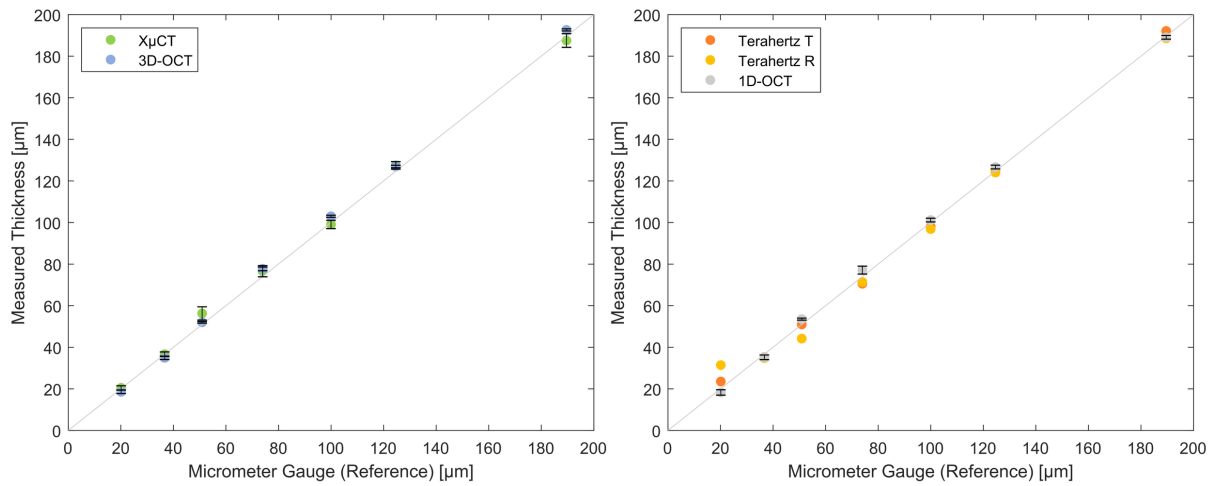
263 3.2 Investigation of PET Foils

264 The experimentally determined film thickness measurements of the Mylar films for the various
 265 methods are summarized in Table 1. Common to all methods is a relatively small standard deviation of
 266 the measured film thickness, which is in most cases lower than the manufacturer's specified tolerance
 267 and the micrometer gauge measurements. For the subsequent analysis, the micrometer gauge method
 268 was applied to represent the reference method for all foils tested. Results that deviated more than
 269 10% from this reference value are highlighted by an asterisk. An illustration of all results is provided in
 270 Figures 1 and 2.

271
 272 Table 1: Comparison of the film thickness measurements acquired using the various methods to determinate the
 273 film thickness of Mylar foils. Results with a deviation of over 10% from the micrometer gauge measurements,
 274 which acted as a reference throughout all measurement, are highlighted by an asterisk.

Foil [μm]	Specification [μm]	Reference [μm]	Terahertz T [μm]	Terahertz R [μm]	X μCT [μm]	3D-OCT [μm]	1D-OCT [μm]
19	19 \pm 1.0	20.1 \pm 2.1	23.5*	31.4*	20.5 \pm 1.0	18.7 \pm 0.8	18.3 \pm 1.3
36	36 \pm 1.8	36.7 \pm 1.8	35.3	34.8	36.7 \pm 1.1	35.2 \pm 0.8	35.2 \pm 1.1
50	50 \pm 2.5	50.9 \pm 1.4	51.0	44.2*	56.3 \pm 3.2*	51.9 \pm 0.4	53.5 \pm 0.5
75	75 \pm 3.8	74.0 \pm 1.1	70.6	71.4	76.6 \pm 2.7	77.6 \pm 0.9	77.1 \pm 1.9
100	100 \pm 5.0	100.0 \pm 1.0	98.0	96.8	99.0 \pm 2.0	103.0 \pm 0.5	101.2 \pm 0.9
125	125 \pm 6.3	124.6 \pm 1.3	125.5	124.0	127.5 \pm 1.8	126.8 \pm 0.6	126.7 \pm 0.9
190	190 \pm 9.5	189.6 \pm 1.9	192.1	188.6	187.5 \pm 3.3	192.5 \pm 0.5	189.1 \pm 0.9
Comment	Specified by manufacturer	Uncertainty: 1.1 μm , k=2 (specification)	Transmission n = 1.765 \pm 0.011	Reflection n = 1.765 \pm 0.011	Voxel size: 1.49 μm	n = 1.615 \pm 0.002	n = 1.615 \pm 0.002

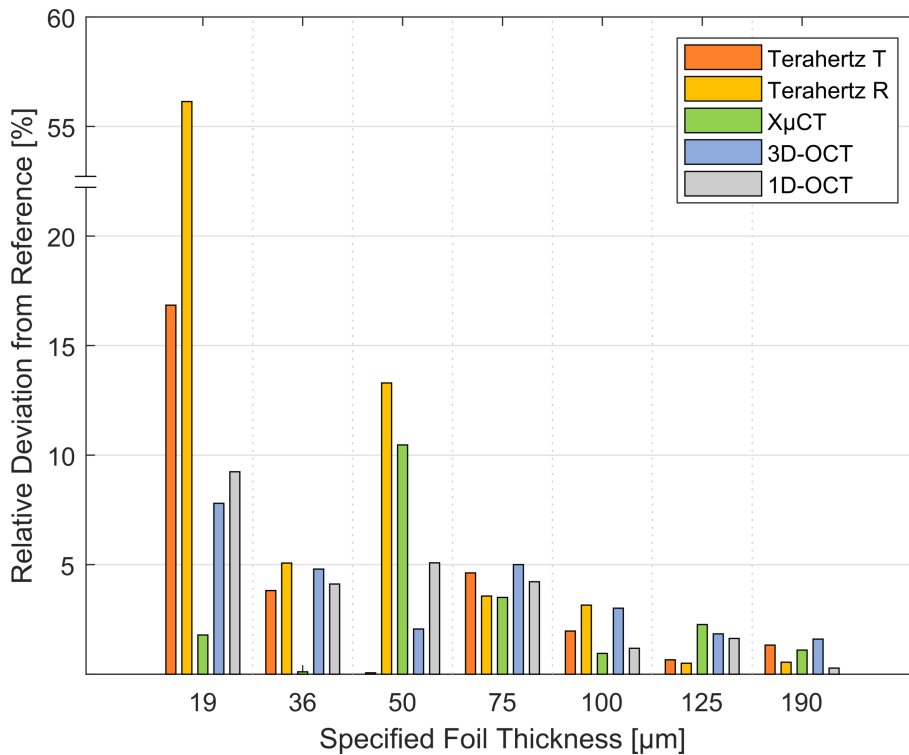
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Figure 1: Comparison of average foil thicknesses with standard deviations in error bars evaluated in relation to micrometer gauge measurements as the reference. Since the terahertz measurements were performed as single-point measurements, no standard deviations are available for them. For the sake of clarity, the 3D and 1D methods are depicted on the left and right sides, respectively.



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Figure 2: Comparison of relative deviations for each method in relation to the reference method (micrometer gauge measurements).

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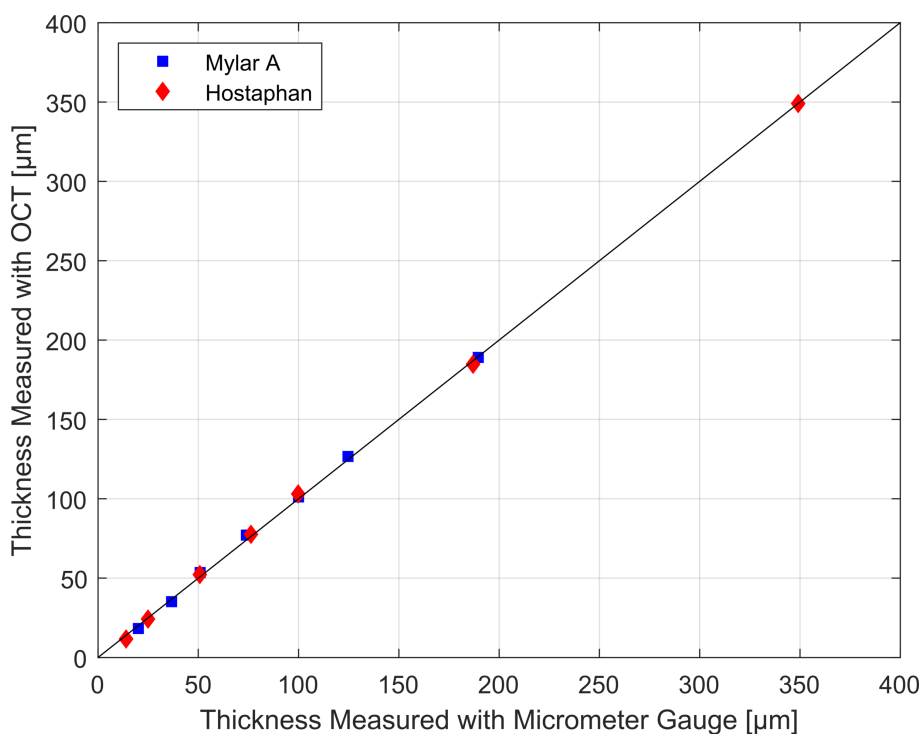
Sample preparation via stacked foils for the $X\mu$ CT measurement facilitates the manual thickness evaluation of the acquired $X\mu$ CT images. $X\mu$ CT and OCT measurements resulted in 3D datasets, and both methods showed that the foils were highly uniform in terms of thickness. The $X\mu$ CT measurements were evaluated by measuring the interface pixel distances using the software ImageJ at 10 different positions per foil. Based on the known voxel size of $1.49 \mu\text{m}$, the corresponding film thickness was calculated. The $X\mu$ CT results show the highest standard deviation among all techniques providing a standard deviation in the chosen setup.

291 Interestingly, only the OCT measurements have a consistently low standard deviation over the entire
 292 thickness range. The results for the OCT measurements indicated good linearity in the thickness range
 293 between 19 μm and 190 μm for Mylar and between 12 μm and 350 μm for the Hostaphan foils.
 294 Coefficients of determination and the root-mean-square error (RMSE) are summarized in Table 2.

295 Table 2: Linearity of methods compared to the micrometer gauge measurements as reference for the Mylar foils.

	Reference	Terahertz T	Terahertz R	X μ CT	3D-OCT	1D-OCT
R²	1.0000	0.9983	0.9864	0.9976	0.9992	0.9989
RMSE [μm]	0.000	2.270	5.283	2.631	2.501	1.999

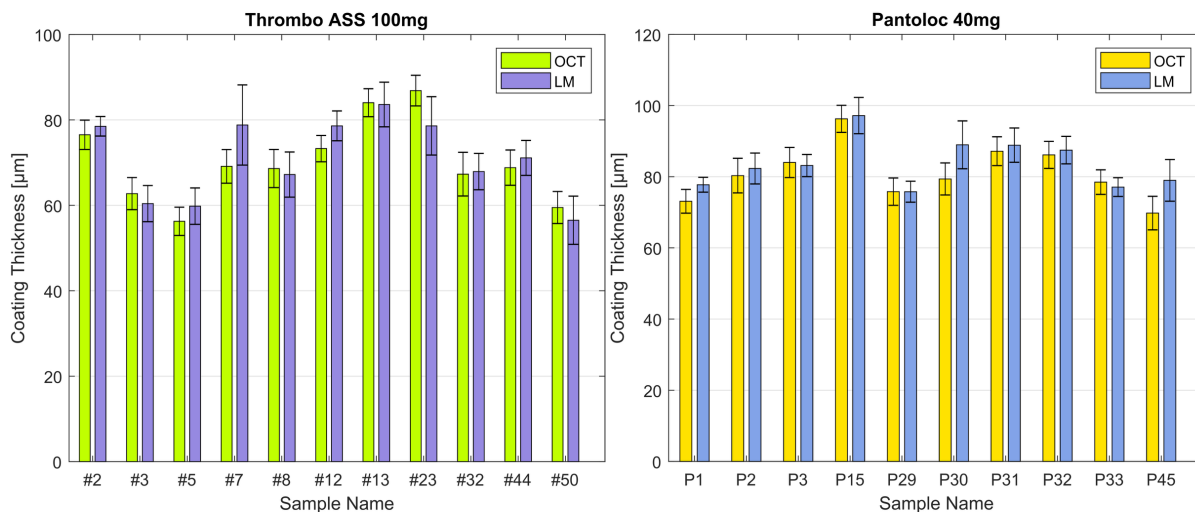
296
 297 A combination of all OCT results for both PET materials in relation to the reference method is provided
 298 in Figure 3. As expected, the linearity is good, even with different PET materials in the same fit and
 299 over a broad thickness range. The coefficient of determination for this mixed set was calculated to be
 300 $R^2 = 0.9993$ and $\text{RMSE} = 2.15 \mu\text{m}$.



301
 302 Figure 3: Comparison of 3-D OCT results for two PET-foils in relation to the reference method over a thickness
 303 range of 12 μm to 350 μm foil thickness. The graph is representative for 1D-OCT as well as for 3D-OCT
 304 measurements. For the sake of clarity only the 3-D data is shown.

305 3.3 Validating Coating Thickness of OCT Measurements performed on coated tablet samples

306 The results for the tablet coating layer thickness measurements for 3D-OCT and light microscopy
 307 measurements are summarized in Figure 4. The OCT and the light microscopy results for
 308 measurements acquired on the same tablet match very well, both for the Thrombo ASS and the
 309 Pantoloc samples.



310

311 Figure 4: Results of average coating thickness and intra-coating variability measured via 3D-OCT and light
 312 microscopy measurements for individual Thrombo ASS and Pantoloc tablets

313 Although both techniques agree well with each other, the variation between tablets of the same type
 314 is unexpectedly high and is resolved both in OCT as well as the microscopy analysis of the cross-
 315 sectional images based on the microtome cuts. Coating thicknesses vary between 56.3 μm to 86.9 μm
 316 for the Thrombo ASS tablets and 69.8 μm to 97.2 μm for the Pantoloc tablets.

317 The results are summarized in Table 3, with additional information about the range of thickness
 318 variations in individual tablets (intra-tablet coating thickness variation). For the automated 1D-OCT
 319 measurements, these values are not deducible using the software applied in this study. The presented
 320 coating variability represent variations of the coating thickness on the tablet cap areas for all three
 321 approaches. Images of tablet edges or the tablet band during acquisition of the rotation drum
 322 measurements were intentionally automated rejected by the 1D system to ensure the same
 323 experimental input conditions for all experiments.

324 Table 3: Results for OCT and light microscopy measurements.

		3D-OCT (manual)	Light Microscopy	1D-OCT (automated)
Thrombo ASS 100mg	Mean [μm]	70.3	71.0	69.0
	SD (<i>inter</i>) [μm]	9.0	8.7	8.3
	SD (<i>intra</i>) [μm]	3.0 – 5.1	2.3 – 9.4	-
Pantoloc 40mg	Mean [μm]	81.0	83.7	81.0
	SD (<i>inter</i>) [μm]	7.3	6.5	7.3
	SD (<i>intra</i>) [μm]	3.3 – 4.9	2.1 – 6.7	-

326

327 4. DISCUSSION

328 4.1 PET Foils as a Validation Material – Comparison of Sensors

329 Reliable micrometer gauge measurements can only be carried out using free-standing, flat films.
 330 Pharmaceutical coatings are neither. They are firmly bonded to the tablet core and have high radii of

331 curvature in many locations on the tablet surface. Another drawback for the caliper method in the
332 context of pharmaceutical film coatings is that it is time-consuming and operator-dependent.
333 However, as a reference for the PET-films this method worked quite well and had an uncertainty of
334 the measurements of 1.1 μm .

335 Among the three technologies suitable for non-destructive and calibration-free examination of tablet
336 coatings tested, terahertz imaging offers the lowest spatial resolution due to the wavelength range
337 applied. Moreover, the estimated resolution limit of about 35 μm agrees with the values in the
338 literature (Zeitler and Gladden, 2009). Regardless of this limitation, the results of terahertz
339 measurements are consistent with the reference and the other technologies tested. For film
340 thicknesses above 36 μm for the transmission and above 50 μm for the reflectance measurements, the
341 deviations from the reference are in the same order of magnitude as the competing technologies. In
342 terms of pharmaceutical coatings, THz imaging has its advantages when it comes to monitoring the
343 tablet coatings with scattering inorganic pigments and high layer thickness exceeding 150 μm . With
344 regard to the PET films as a reference material, the THz results are plausible and indicate good linearity,
345 even when considering the results below the resolution limit.

346 The X-ray microcomputer tomography ($X\mu\text{CT}$) measurements correlate well with the reference
347 method, although the measured thickness tends to be slightly higher, as well as the SDs. This is
348 surprising, as $X\mu\text{CT}$ is considered a "gold standard" and a considerably long measurement time in
349 combination with the technical effort suggests a higher accuracy of the results. Nevertheless, $X\mu\text{CT}$ has
350 the highest spatial resolution of the methods tested and offers full 3D volume information, including
351 microstructural features that are not visible via OCT or THz. With regard to the PET films, the $X\mu\text{CT}$
352 measurements agree well with the competing technologies, additionally showing that the various
353 degrees of film thickness have the same microstructure. Tomograms of $X\mu\text{CT}$ and 3D OCT
354 measurements underline a high uniformity of the films in terms of thickness.

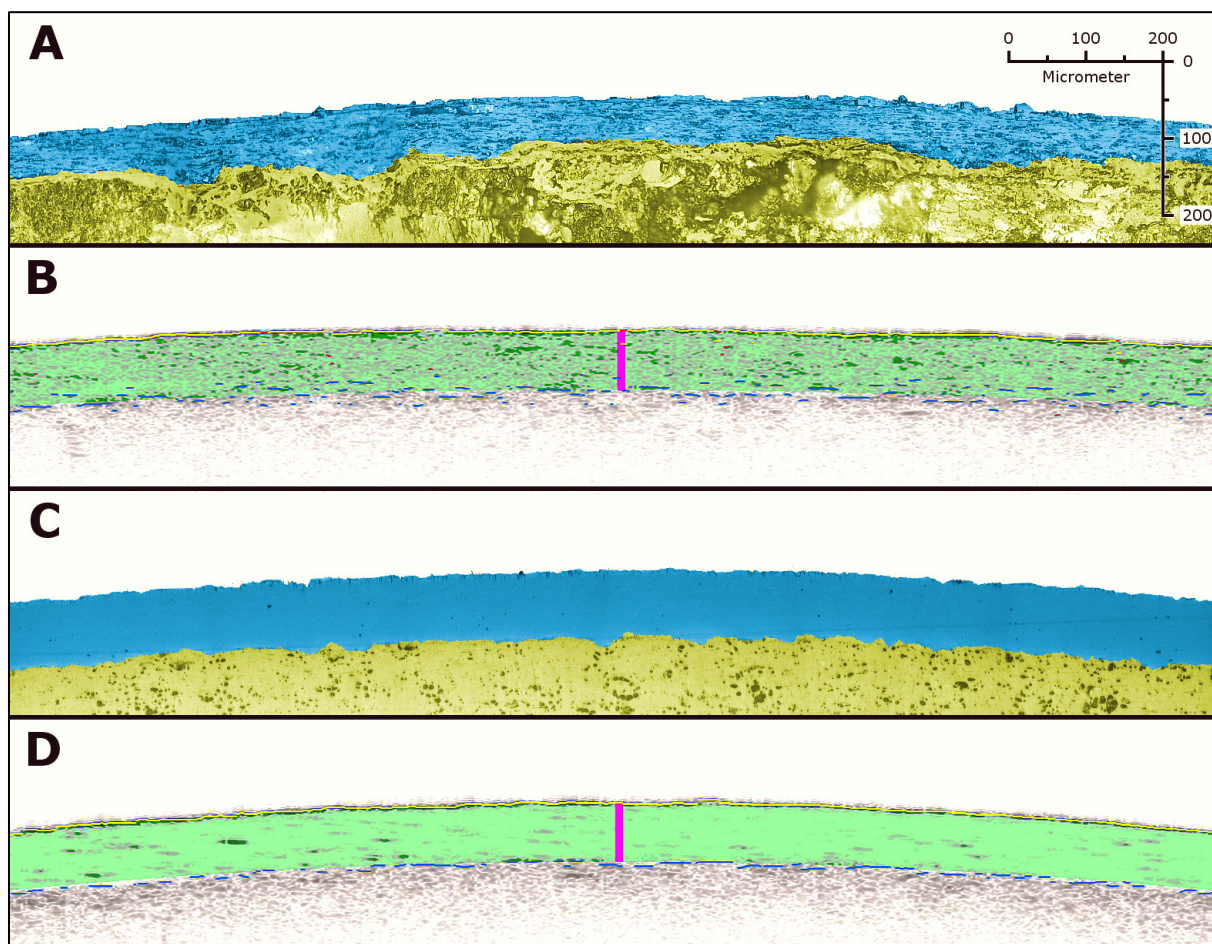
355 The OCT measurements agree very well with the reference and other methods. Particularly
356 noteworthy are the constant low standard deviations for both 1D- and 3D-OCT measurements, which
357 emphasize the high optical quality and homogeneity of the films and equipment used. The linearity of
358 tested OCT systems was investigated for two different polyesters over wide thickness ranges of 19-
359 190 μm for Mylar and 12-390 μm for Hostaphan, respectively, indicating excellent linearity and
360 correlation with the reference method over the whole thickness range. The performance of our in-
361 house prototype is comparable with the commercial OSeeT system, except for the convenience during
362 operation and time effort for the measurements and evaluation of the commercial system.

363 The proposed approach of using PET foils as a validation target cannot replace the established
364 reference targets, such as e.g. the Arden Photonics reference target for ultra-high resolution OCTs
365 (UHR-OCTs) or for the measurement of point-spread-function and lateral resolution. However, it offers
366 a very simple and reliable system for, even fully automated, performance verification and validation
367 of industrial OCT systems.

368 *4.2 Comparison of Reported Tablet Coating Thicknesses - Light Microscopy vs. OCT*

369 The results for the light microscopy and OCT measurements correlate very well for both Thrombo ASS
370 and Pantoloc tablets. The standard deviations are in the same range for both techniques except for
371 the samples #7, #23 (Thrombo ASS) and P30 (Pantoloc). Comparing the results based on individual
372 tablets, the performance of OCT and light microscopy (LM) is very consistent. However, the variation

373 between single tablets (inter-tablet coating thickness variation) is pronounced, with coating
374 variabilities of 12.8% RSD (OCT) and 12.5% RSD (LM) for Thrombo ASS and 9.0% RSD (OCT) and 7.7%
375 RSD (LM) for Pantoloc. Since the tablets tested are commercial tablets from a pharmacy and at least
376 the Thrombo ASS tablets are all from one box and, according to the batch code on the blisters, from
377 one batch, this high variation reflects the real variation in the existing coating processes. These findings
378 are supported by the microscopy images in Figure 5, with a high variation of coating thickness along
379 the intersection of the tablet. They are consistent with the literature for both in-line and off-line
380 measurements of tablet coatings (Sacher et al., 2019; Wolfgang et al., 2019).



381
382 Figure 5: Detail of various Thrombo ASS (A, B) and Pantoloc tablets (C, D) recorded with light microscopy (A, C)
383 and 3D-OCT (B, D). The intersection of A and C is presented by stitched microscopy images. Note a strong
384 variation in the coating thickness, especially in A. For better visualization, the core is shaded yellow and the
385 enteric coating blue for the light microscopy images. For the OCT images (B, D) the green band and the pink bar
386 correspond to the features extracted via the automated evaluation algorithm. The scale is the same for all
387 pictures.

388 As stated in the Material and Methods section and shown in Figure 5, no attempt to perfectly co-locate
389 A, B and C, D were made, but the respective locations are very close to each other. The strong variation
390 in Thrombo ASS picture (A) is not so obvious in the corresponding 3D-OCT image due to the overlay of
391 the algorithmic features and strong scattering of the enteric coating containing a high amount of talc
392 (approximately 30% talc in the dry coating according to technical notes on this coating system (Evonik
393 Industries AG, 2014)).

394 The microscopy image evaluation was made manually by measuring the coating thickness in regular
395 intervals over the entire cutting edge, as described in the materials and methods section. This resulted
396 in a small number of measurements of 7-18 per sample, depending on the interface length available.
397 In contrast, the automated evaluated 1D OCT measurements had a pre-set standardized measuring
398 routine and only reported the tablet value when at least 50 measurements per interface or more were
399 detected. Based on these data, a statistical evaluation of the readings can be performed. The 1D-OCT
400 system evaluates the complete variation of a contiguous portion of the cross sections in the scanned
401 area and calculates the coating thickness and its variation, as well the optical homogeneity of the layer
402 and the surface roughness like presented by Markl et al. (Markl et al., 2018).

403 Comparing both techniques, the results demonstrate that OCT (1D and 3D) and light microscopy
404 deliver consistent results. The OCT measurements seem to be more plausible in terms of a statistically
405 sounder basis, especially for the automated 1D measurements, and can be performed destruction free,
406 calibration free and within a few minutes. Our work demonstrates that automatically evaluated OCT
407 measurements of commercial pharmaceutical coatings withstand a critical comparison with
408 established technology for coating thickness evaluation.

409 **5. SUMMARY AND CONCLUSIONS**

410 This study demonstrates that biaxially stretched polyethylene terephthalate films can be applied ~~(even~~
411 ~~in an industrial environment)~~ to compare system performance of various sensor systems in terms of
412 thickness measurements. Among the technologies tested, OCT appears to provide the most consistent
413 results compared to the established reference methods. Due to the physical and chemical material
414 properties and the applicability to all tested sensors, PET films can be considered an excellent model
415 system for validating the measuring instruments for monitoring purposes in the pharmaceutical
416 industry. Moreover, we believe that PET foils could serve in the future as a very economic and easy to
417 use layer thickness standard for medical OCT applications too.

418 The comparison of measured coating thickness and its variation via 1D- and 3D-OCT as well as light
419 microscopy on commercially-available tablets demonstrates the advantages and reliability of OCT. All
420 results of 3D-OCT measurements and LM correlate very well. Fully automatic measurements and
421 evaluation via 1D-OCT reports the same results as the reference method (LM) in a much shorter time.
422 In addition, OCT measurements can provide further information about pharmaceutical coatings, such
423 as surface roughness, defects and optical film homogeneity in real-time like presented in (Sacher et
424 al., 2019).

425 Our results indicate that OCT can be used in the pharmaceutical industry for generating significant
426 statistical data of mean coating thickness with information about inter- and intra-tablet coating
427 thickness variability. Thus, OCT enables scientists and process engineers to achieve an enhanced
428 understanding of the critical quality attributes of pharmaceutical coatings in real-time, including
429 thickness, variability and coating quality, both intra- and inter-batch.

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437

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